

Study of heat transfer in Cartesian, cylindrical and spherical geometries

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Outline

- Boltzmann equation with respect to arbitrary coordinates
- Boltzmann equation with respect to orthonormal vielbein fields
- Gauss-Hermite quadratures
- Heat transfer in cartesian, cylindrical and spherical symmetric geometries
 - Hydrodynamic, transition and free molecular flow regimes

Boltzmann equation

- Evolution equation of the one-particle distribution function f with respect to the Cartesian coordinates:

$$\frac{\partial f}{\partial t} + \frac{p^i}{m} \frac{\partial f}{\partial x^i} + F^i \frac{\partial f}{\partial p^i} = J[f]. \quad (1)$$

- Hydrodynamic moments of order N give macroscopic quantities:

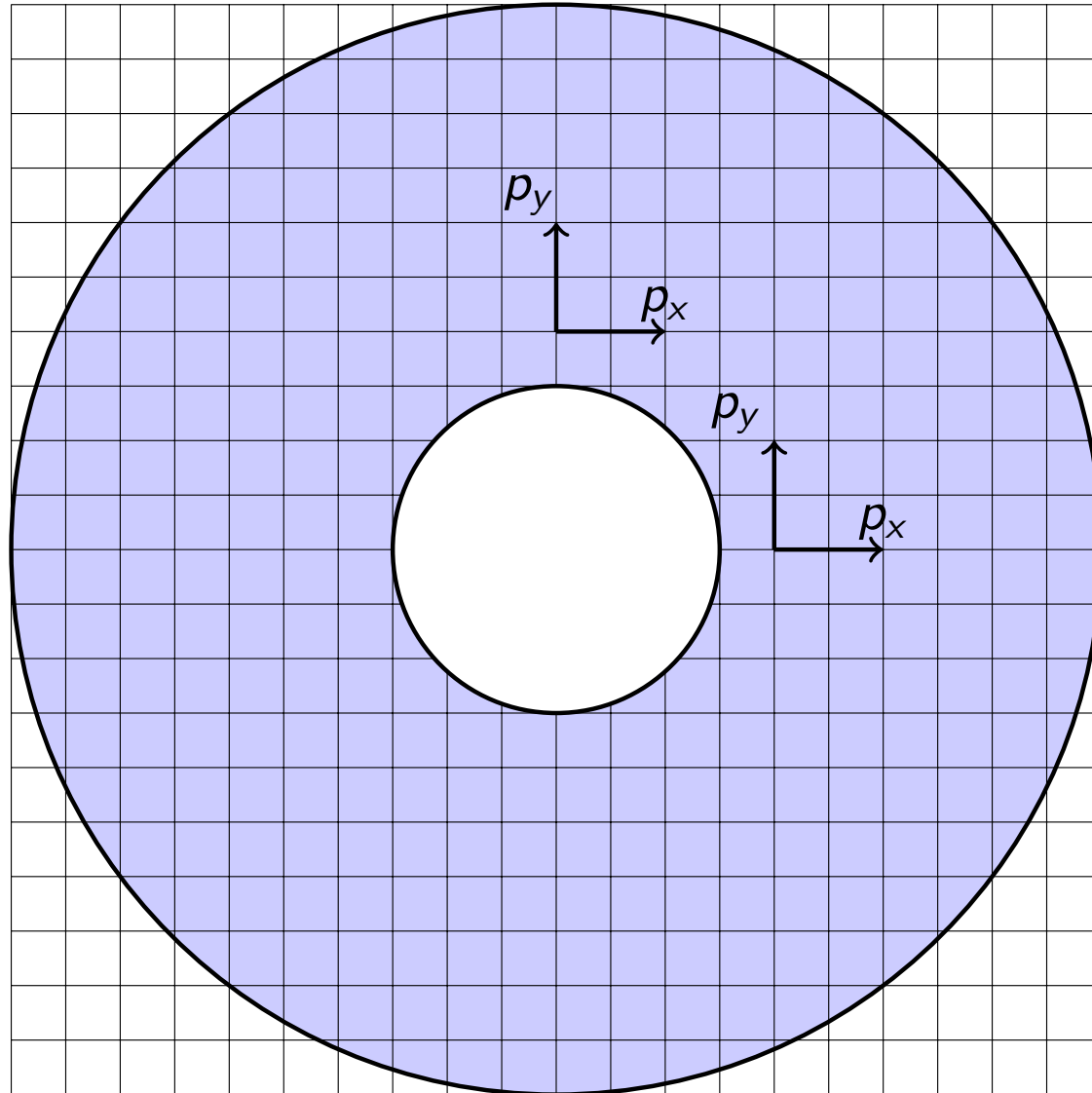
$$N=0 : \quad \text{number density:} \quad n = \int d^3 p f,$$

$$N=1 : \quad \text{velocity:} \quad \mathbf{u} = \frac{1}{nm} \int d^3 p f \mathbf{p},$$

$$N=2 : \quad \text{temperature:} \quad T = \frac{2}{3n} \int d^3 p f \frac{\xi^2}{2m}, \quad (\xi = \mathbf{p} - m\mathbf{u}),$$

$$N=3 : \quad \text{heat flux:} \quad \mathbf{q} = \frac{1}{2m^2} \int d^3 p f \xi^2 \xi.$$

Cartesian grid and momentum space decomposition along the Cartesian axes.



Boltzmann equation - arbitrary coordinates

- Consider a coordinate transformation $x^i \rightarrow x^{\tilde{i}}$, which induces a metric $g_{\tilde{i}\tilde{j}}$, as follows:

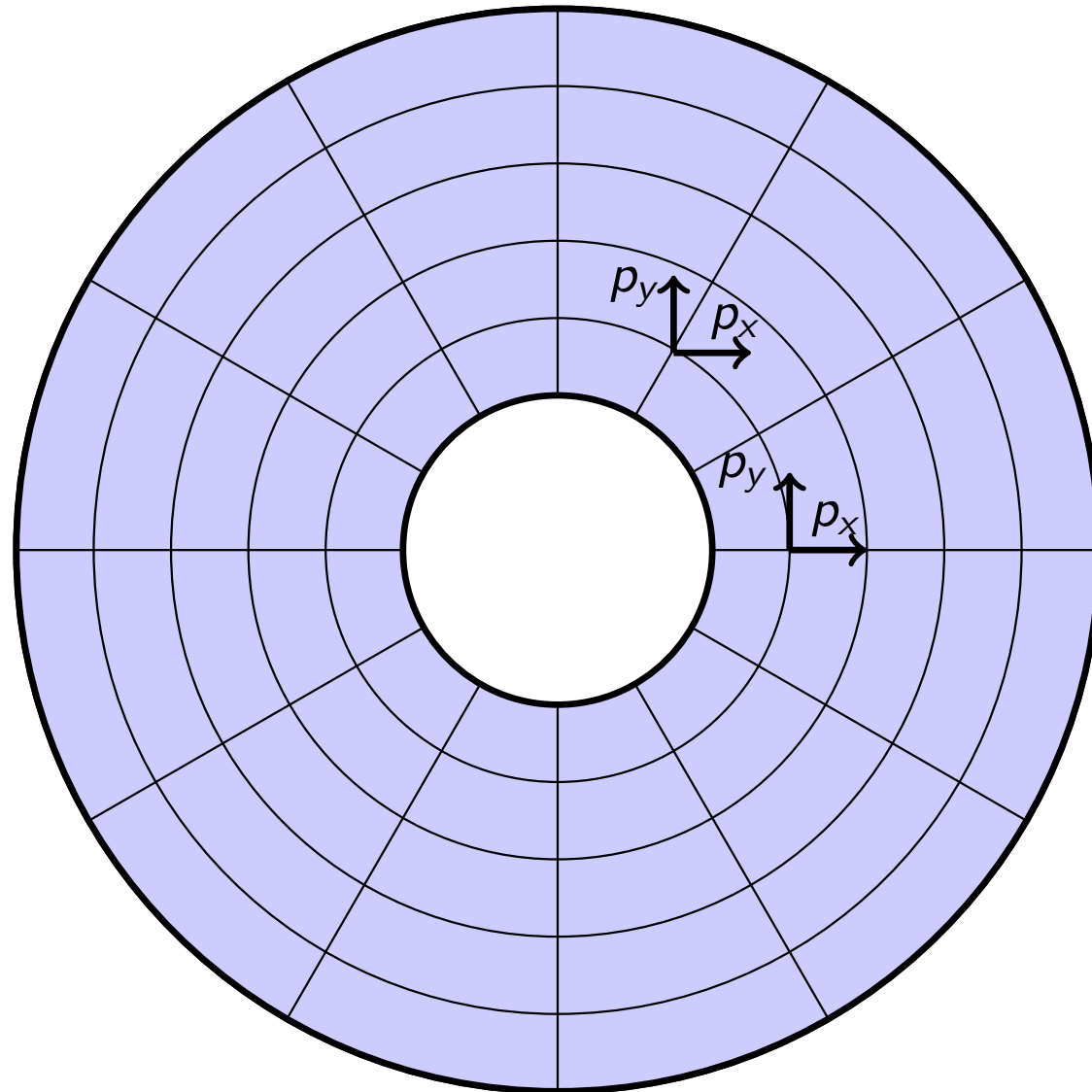
$$ds^2 = \delta_{ij} dx^i dx^j = g_{\tilde{i}\tilde{j}} dx^{\tilde{i}} dx^{\tilde{j}},$$

$$g_{\tilde{i}\tilde{j}} = \delta_{ij} \frac{\partial x^i}{\partial x^{\tilde{i}}} \frac{\partial x^j}{\partial x^{\tilde{j}}}.$$

- The Boltzmann equation with respect to the new spatial coordinates reads:

$$\frac{\partial f}{\partial t} + \frac{p^i}{m} \frac{\partial x^{\tilde{i}}}{\partial x^i} \frac{\partial f}{\partial x^{\tilde{i}}} + F^i \frac{\partial f}{\partial p^i} = J[f]. \quad (2)$$

Cylindrical grid and momentum space decomposition along the Cartesian axes



Boltzmann equation - orthonormal vielbein fields

- Furthermore, we note that:

$$p^{\tilde{i}} = p^i \frac{\partial x^{\tilde{i}}}{\partial x^i}, \quad F^{\tilde{i}} = F^i \frac{\partial x^{\tilde{i}}}{\partial x^i}, \quad \mathbf{p}^2 \equiv g_{\tilde{i}\tilde{j}} p^{\tilde{i}} p^{\tilde{j}}$$

- By introducing the triad vector frame and the associated one-form co-frame:

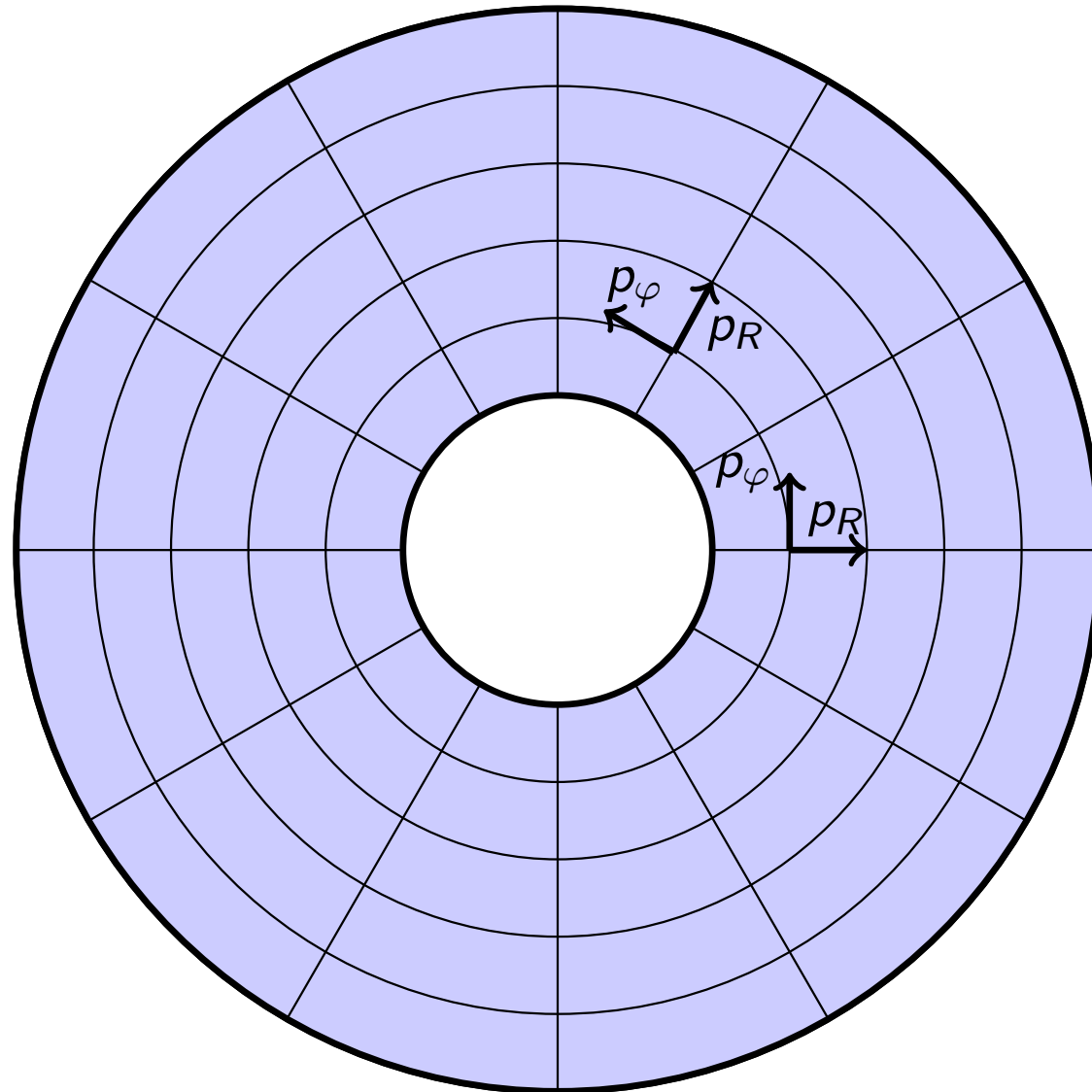
$$e_{\hat{a}} = e_{\hat{a}}^{\tilde{i}} \partial_{\tilde{i}}, \quad \omega^{\hat{a}} = \omega_{\tilde{i}}^{\hat{a}} dx^{\tilde{i}}, \quad g_{\tilde{i}\tilde{j}} dx^{\tilde{i}} dx^{\tilde{j}} = \delta_{\hat{a}\hat{b}} \omega^{\hat{a}} \omega^{\hat{b}}$$

the inner product $\mathbf{p}^2 \equiv \delta_{\hat{a}\hat{b}} p^{\hat{a}} p^{\hat{b}}$ is decoupled from the metric.

- The Boltzmann equation reads:

$$\frac{\partial f}{\partial t} + \frac{p^{\hat{a}}}{m} e_{\hat{a}}^{\tilde{i}} \frac{\partial f}{\partial x^{\tilde{i}}} + \left(F^{\hat{a}} - \frac{1}{m} \Gamma^{\hat{a}}_{\hat{b}\hat{c}} p^{\hat{b}} p^{\hat{c}} \right) \frac{\partial f}{\partial p^{\hat{a}}} = J[f], \quad (3)$$

Cylindrical grid and momentum space decomposition adapted to the curvilinear coordinates.



Cylindrical coordinates

- The line element in cylindrical coordinates and the associated triad are:

$$ds^2 = dR^2 + R^2 d\varphi^2 + dz^2, \quad e_{\hat{R}} = \partial_R, \quad e_{\hat{\varphi}} = R^{-1} \partial_{\varphi}, \quad e_{\hat{z}} = \partial_z. \quad (4)$$

- The Boltzmann equation when the flow is homogeneous w.r.t. φ and z reads:

$$\frac{\partial f}{\partial t} + \frac{2p^{\hat{R}}}{m} \frac{\partial(fR)}{\partial R^2} + \frac{1}{mR} \left[(p^{\hat{\varphi}})^2 \frac{\partial f}{\partial p^{\hat{R}}} - p^{\hat{R}} \frac{\partial(fp^{\hat{\varphi}})}{\partial p^{\hat{\varphi}}} \right] = -\frac{1}{\tau} (f - f^{(\text{eq})}). \quad (5)$$

- The advection term is implemented following Falle et al.¹

¹S. A. E. G. Falle and S. S. Komissarov, Mon. Not. R. Astron. Soc. **278**, 586-602 (1996).

Spherical coordinates

- The line element in spherical coordinates and its associated triad are:

$$ds^2 = dR^2 + R^2(d\theta^2 + \sin^2 \theta d\varphi^2), \quad e_{\hat{R}} = \partial_R, \quad e_{\hat{\theta}} = \frac{\partial \theta}{R}, \quad e_{\hat{\varphi}} = \frac{R^{-1}}{\sin \theta} \partial_{\varphi}. \quad (6)$$

- Assuming that the flow is homogeneous w.r.t. θ and φ , the Boltzmann equation reads:

$$\begin{aligned} \frac{\partial f}{\partial t} + \frac{3p^{\hat{R}}}{m} \frac{\partial(fR^2)}{\partial R^3} + \frac{1}{mR} \left[\left((p^{\hat{\theta}})^2 + (p^{\hat{\varphi}})^2 \right) \frac{\partial f}{\partial p^{\hat{R}}} - p^{\hat{R}} \left(\frac{\partial(f p^{\hat{\theta}})}{\partial p^{\hat{\theta}}} + \frac{\partial(f p^{\hat{\varphi}})}{\partial p^{\hat{\varphi}}} \right) \right] \\ = -\frac{1}{\tau} (f - f^{(\text{eq})}). \quad (7) \end{aligned}$$

- The advection term is implemented following Downes et al.²

²T. P. Downes, P. Duffy and S. S. Komissarov, Mon. Not. R. Astron. Soc. 332, 144–154 (2002).

Coordinates stretching

$$\text{Let } R(\eta) = R_{\text{in}} + (R_{\text{out}} - R_{\text{in}}) \left(\delta + \frac{A_0}{A} \tanh \eta \right), \quad A_0 = \max(\delta, 1 - \delta). \quad (8)$$

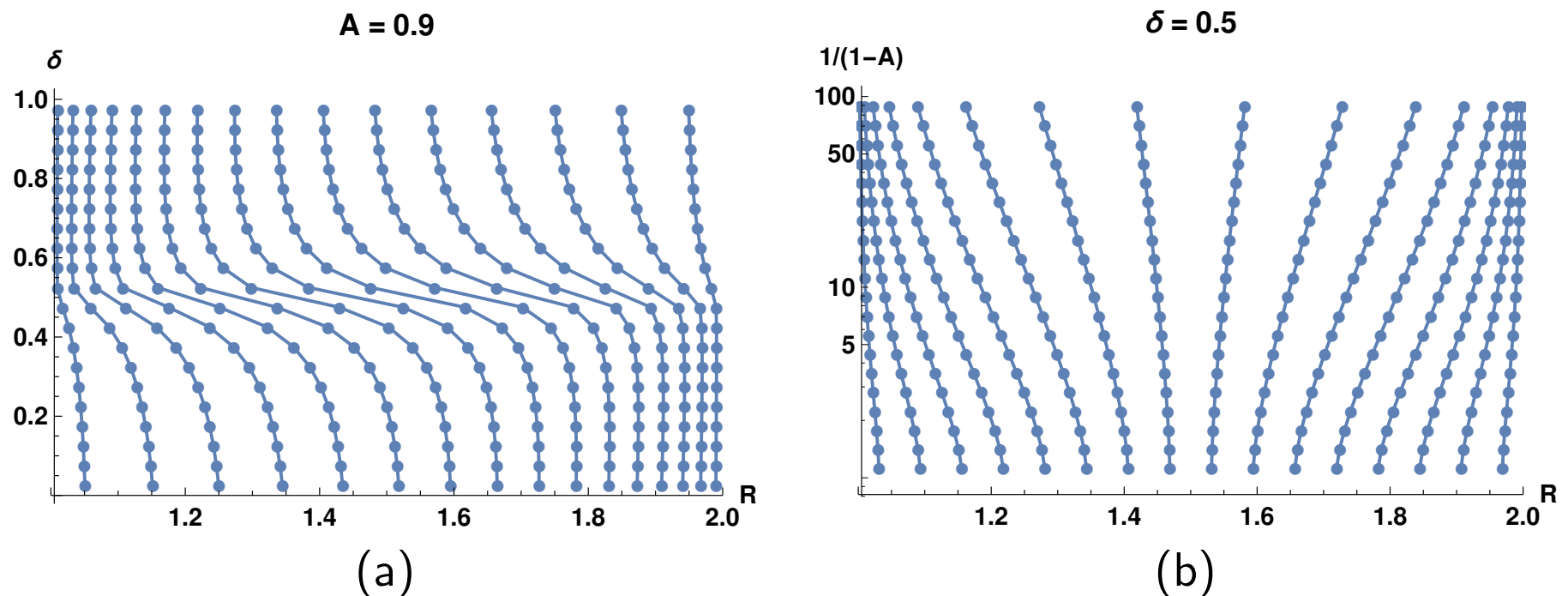


Figure 1: Effect of grid stretching on 16 points between $R_{\text{in}} = 1$ and $R_{\text{out}} = 2$.

(a) The parameter $\delta \in (0, 1)$ controls the positioning of the stretching centre.

(b) The parameter $A \in (0, 1)$ contains the amplitude of the stretching.

The points are equidistant in η .

Lattice Boltzmann - Gauss-Hermite quadratures

- The numerical models employed are mixed quadrature lattice Boltzmann³. f and $f^{(eq)}$ are expanded with respect to Hermite(HLB) and Half-Range Hermite(HHLB) polynomials, e. g.(1D case):

$$f_i^{eq}(\mathbf{x}, t) = w_i \sum_{\ell=0}^N \frac{1}{\ell!} \mathbf{a}_{(\ell)}^{eq}(\mathbf{x}, t) \mathcal{H}^{(\ell)}(p_i)$$

- 3D model = 1D $\times$ 1D $\times$ 1D.
- We will denote such models by: HHLB(Q_R) $\times$ HLB(Q_φ) $\times$ HLB(Q_z).
- The moments of the distribution function are evaluated as:

$$\int d^3\hat{p} f p^{\hat{a}_1} \dots p^{\hat{a}_s} = \sum_{i=1}^{Q_R} \sum_{j=1}^{Q_\varphi} \sum_{k=1}^{Q_z} f_{ijk} \prod_{\ell=1}^s p_{ijk}^{\hat{a}_\ell}. \quad (9)$$

Here $Q_\alpha, \alpha \in \{R, \varphi, z\}$ represents the quadrature order.

³V.E. Ambrus and V. Sofonea, J. Comput. Phys. **316**, 760-788 (2016)

Force term

Boltzmann equation written for the discrete distributions f_{ijk} :

$$\frac{\partial f_{ijk}}{\partial t} + \frac{2p_i^{\hat{R}}}{m} \frac{\partial(f_{ijk}R)}{\partial R^2} + \frac{1}{mR} \left\{ (p_j^{\hat{\phi}})^2 \left(\frac{\partial f}{\partial p^{\hat{R}}} \right)_{ijk} - p_i^{\hat{R}} \left[\frac{\partial(f p^{\hat{\phi}})}{\partial p^{\hat{\phi}}} \right]_{ijk} \right\} = -\frac{1}{\tau} (f_{ijk} - f_{ijk}^{(\text{eq})})$$

- We write the terms involving the derivative of f as follows⁴ :

$$\left(\frac{\partial f}{\partial p^{\hat{R}}} \right)_{ijk} = \sum_{i'=1}^{Q_R} \mathcal{F}_{i,i'}^R f_{i'jk},$$

- The matrix $\mathcal{F}_{k,j}^R$ has the following form:

$$\mathcal{F}_{k,j}^R = -w_k^H \sum_{\ell=0}^{Q-1} \frac{1}{\ell!} H_{\ell+1}(p_k) H_{\ell}(p_j)$$

⁴V. E. Ambruş, V. Sofonea, R. Fournier, and S. Blanco, *Implementation of the force term in half-range lattice Boltzmann models*, in preparation.

Lattice Boltzmann - Numerical scheme

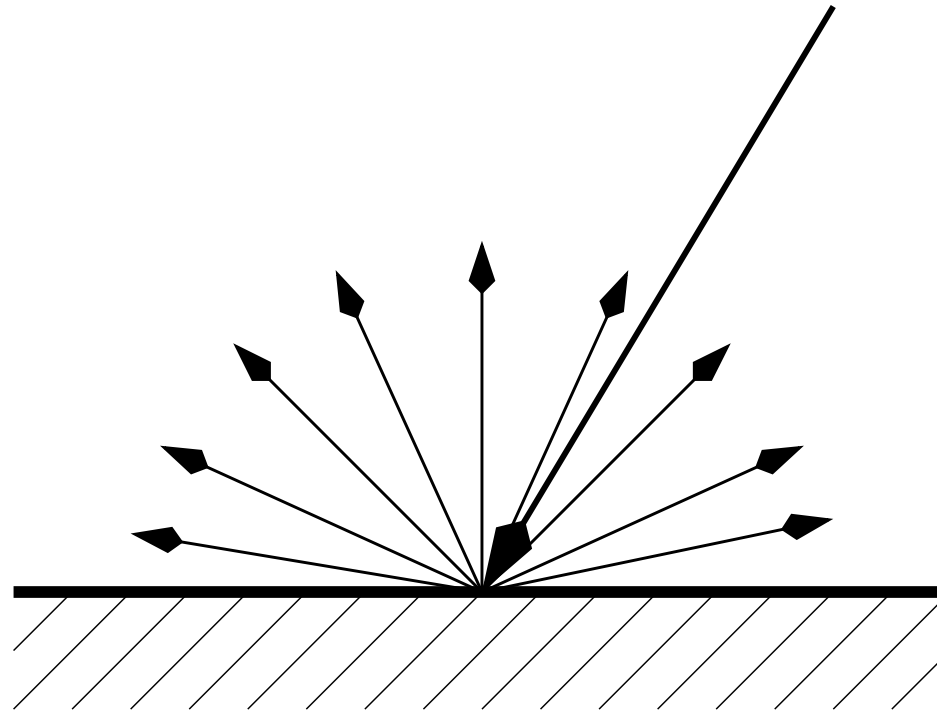
- Velocity vectors are given by the roots of the Hermite/Half-Range Hermite polynomials.
- The roots are irrational numbers for a quadrature order $Q > 2$ which implies a off-lattice velocity set.
- Time-stepping: TVD RK3⁵
- Advection: The fifth order WENO-5 scheme⁶.

⁵C.-W. Shu and S. Osher, J. Comput. Phys. 77, 439–471 (1988).

⁶G. S. Jiang and C. W. Shu, J. Comput. Phys. 126, 202 (1996).

Diffuse reflection boundary conditions

- Reflected particles carry some information that belongs to the wall.

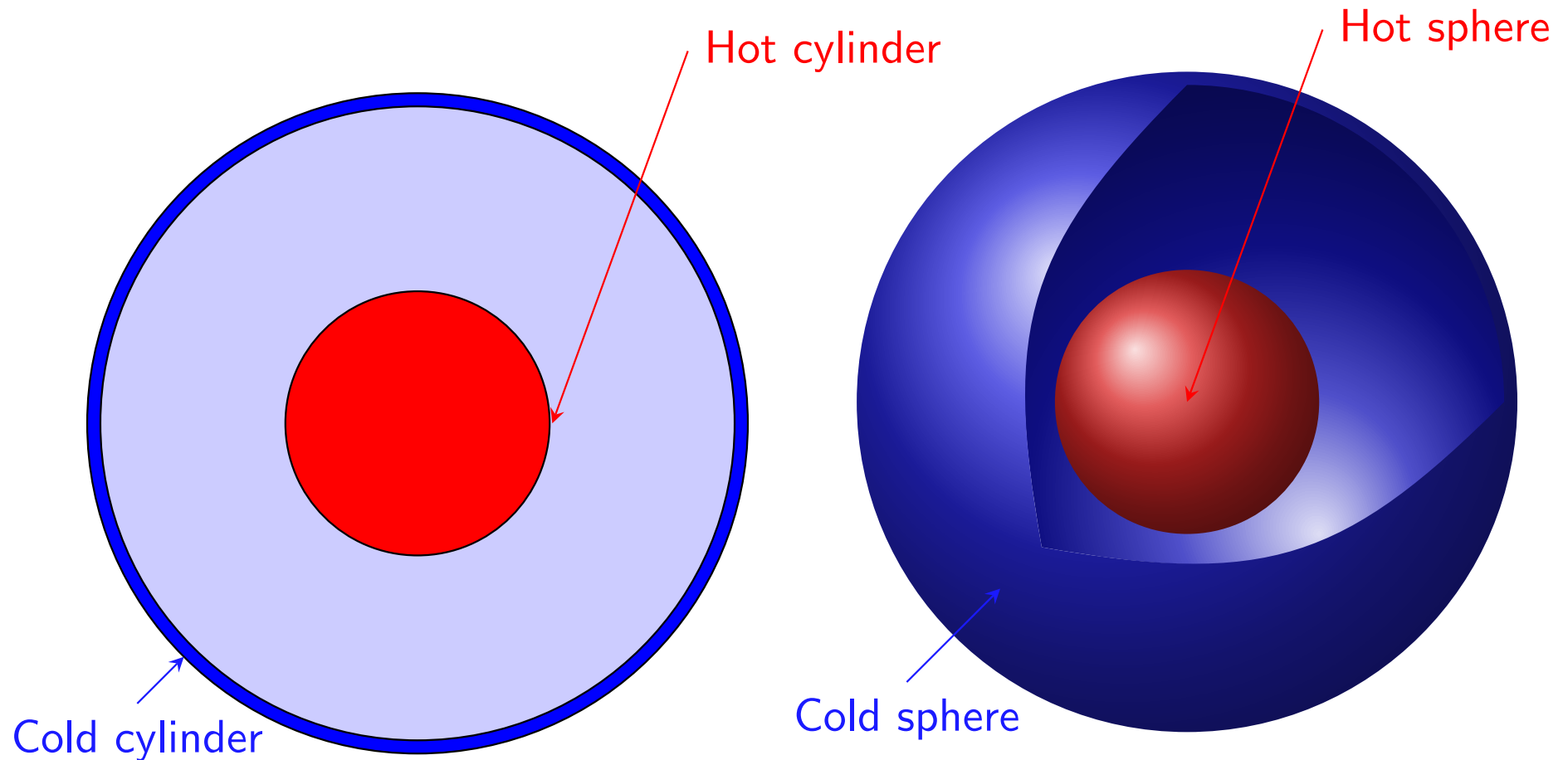


diffuse reflection

- The density n_w is fixed by imposing zero flux through the boundary:

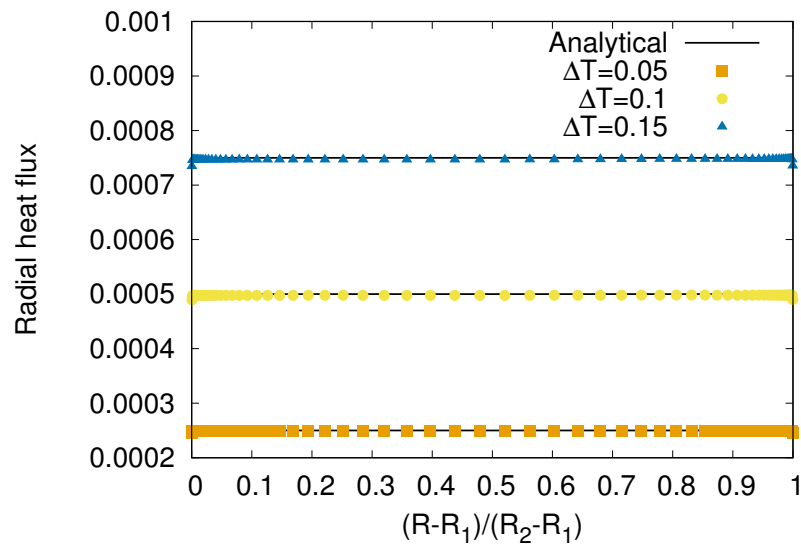
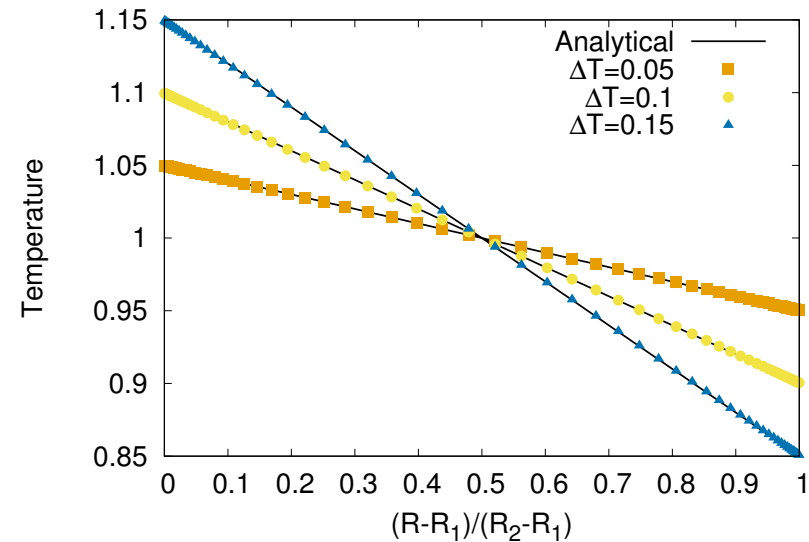
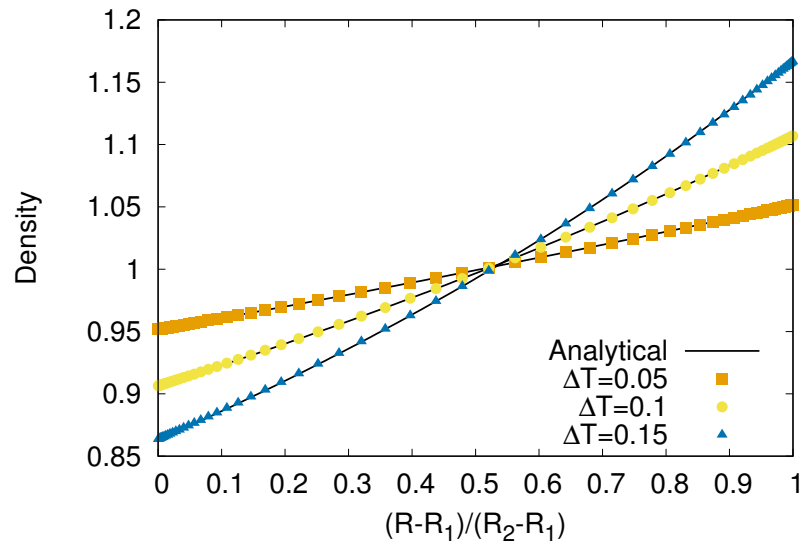
$$\int_{\mathbf{p} \cdot \boldsymbol{\chi} > 0} d^3 p f(\mathbf{p} \cdot \boldsymbol{\chi}) = - \int_{\mathbf{p} \cdot \boldsymbol{\chi} < 0} d^3 p f^{(\text{eq})}(\mathbf{p} \cdot \boldsymbol{\chi}).$$

Heat transfer - cartesian, cylindrical and spherical symmetry



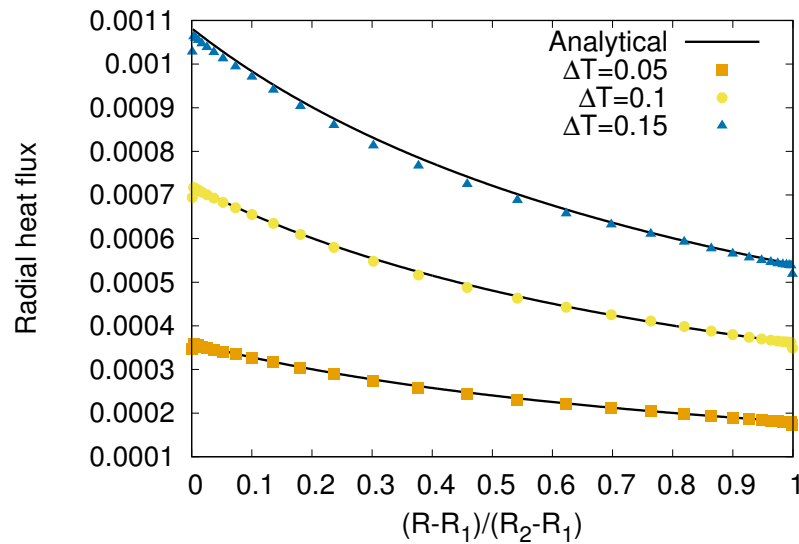
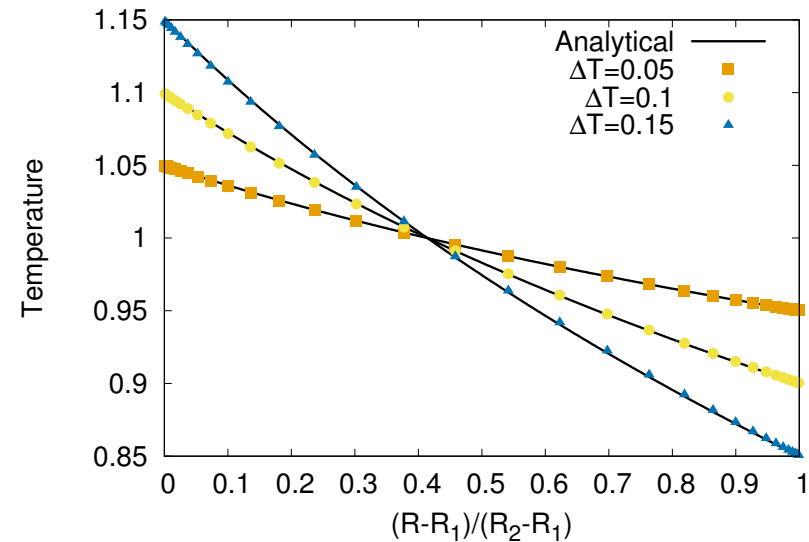
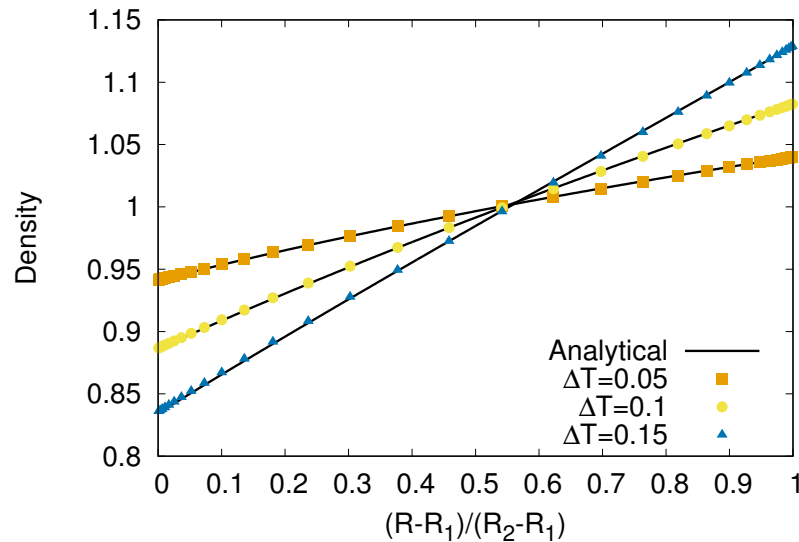
$$T_{hot/cold} = T \pm \Delta T$$

Parallel plates $Kn \rightarrow 0$



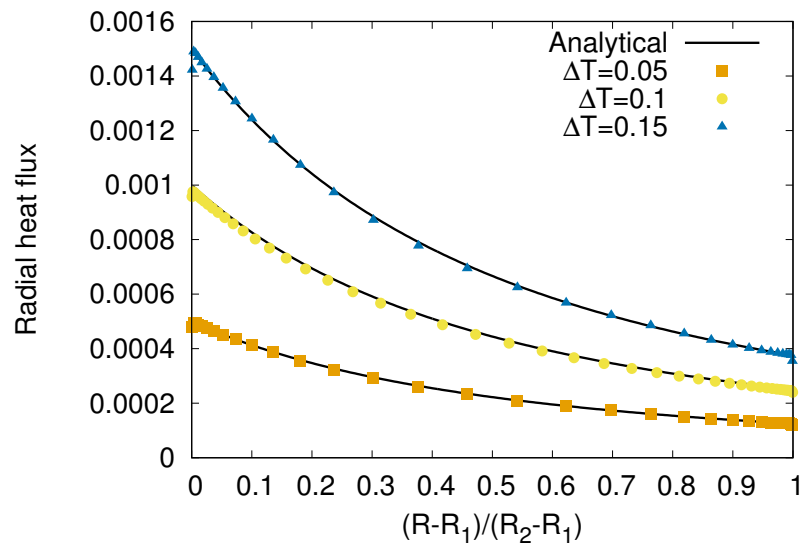
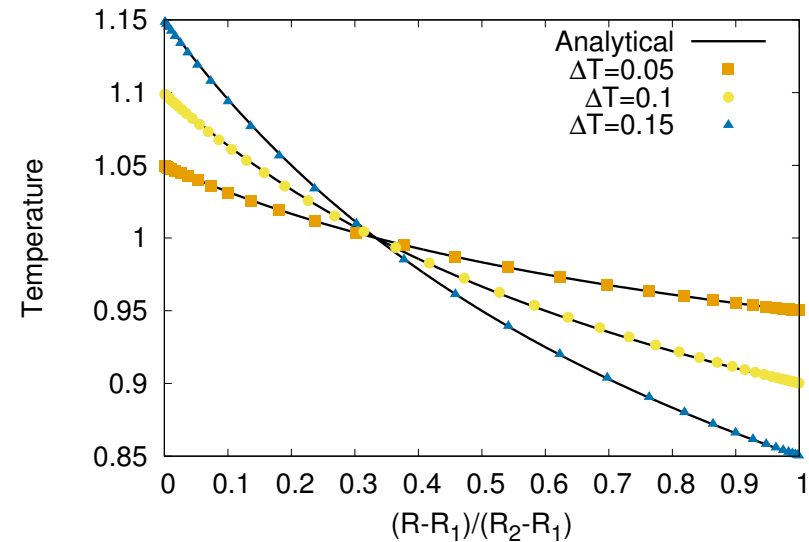
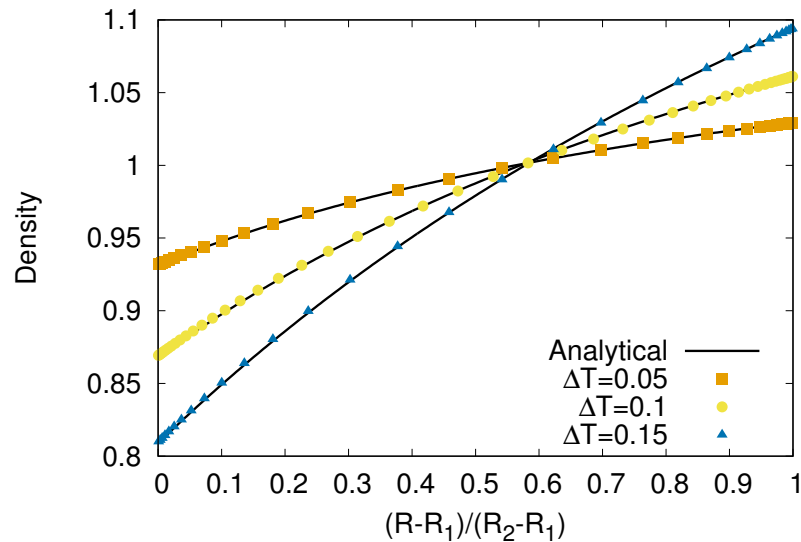
Profiles of number density, temperature for a wall temperature spread $\Delta T = 0.05, 0.1, 0.15$.

Cylindrical symmetry $Kn \rightarrow 0$



Profiles of number density, temperature for a wall temperature spread $\Delta T = 0.05, 0.1, 0.15$.

Spherical symmetry $Kn \rightarrow 0$



Profiles of number density, temperature for a wall temperature spread $\Delta T = 0.05, 0.1, 0.15$.

Parallel plates - transition regime

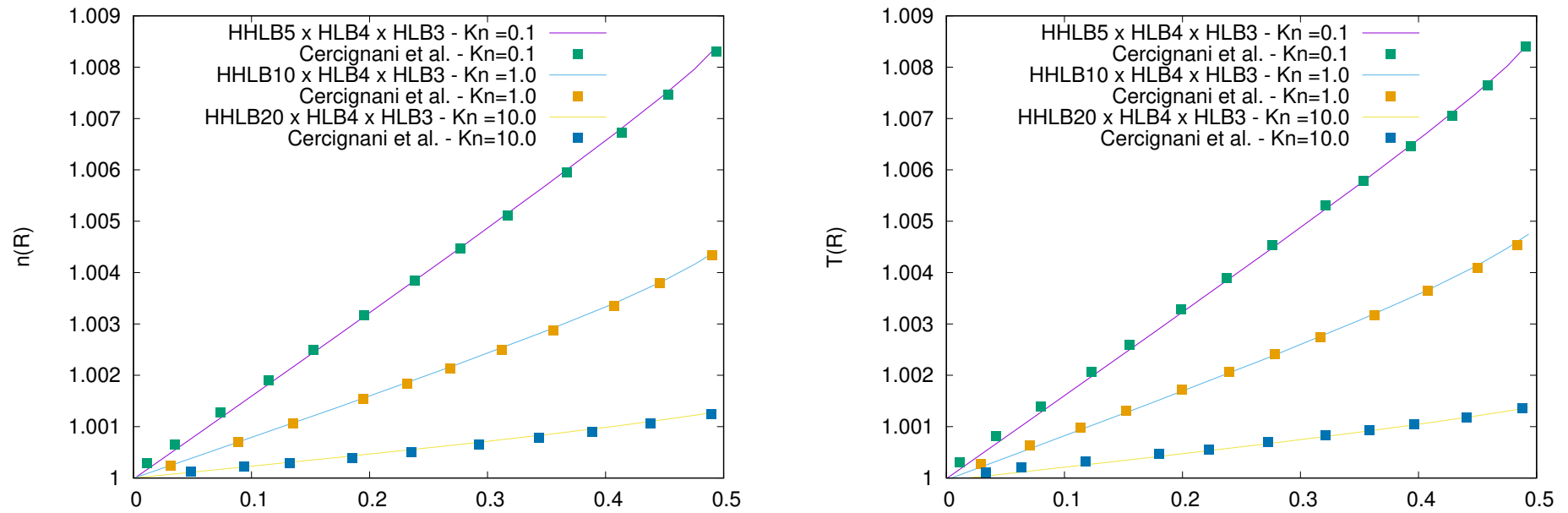


Figure 2: Half domain heat transfer comparison with the study of Bassanini et al.⁷

⁷P. Bassanini, C. Cercignani and C. D. Pagani, Int.J. Heat Transfer, Vol. 10, pp. 447-460. 1967

Parallel plates - transition regime

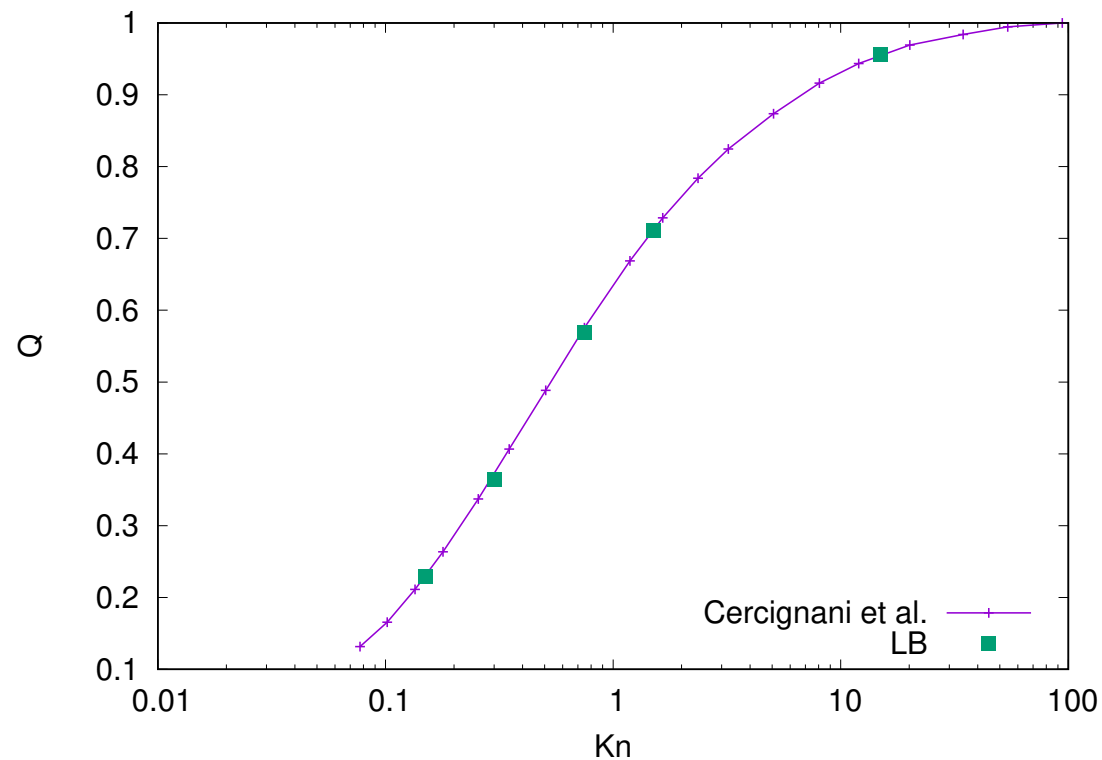


Figure 3: Q constant comparison with the study of Bassanini et al.⁸.
 $Q=q(R)=\text{const.}$

⁸P. Bassanini, C. Cercignani and C. D. Pagani, Int.J. Heat Transfer, Vol. 10, pp. 447-460. 1967

Cylindrical Symmetry - transition regime

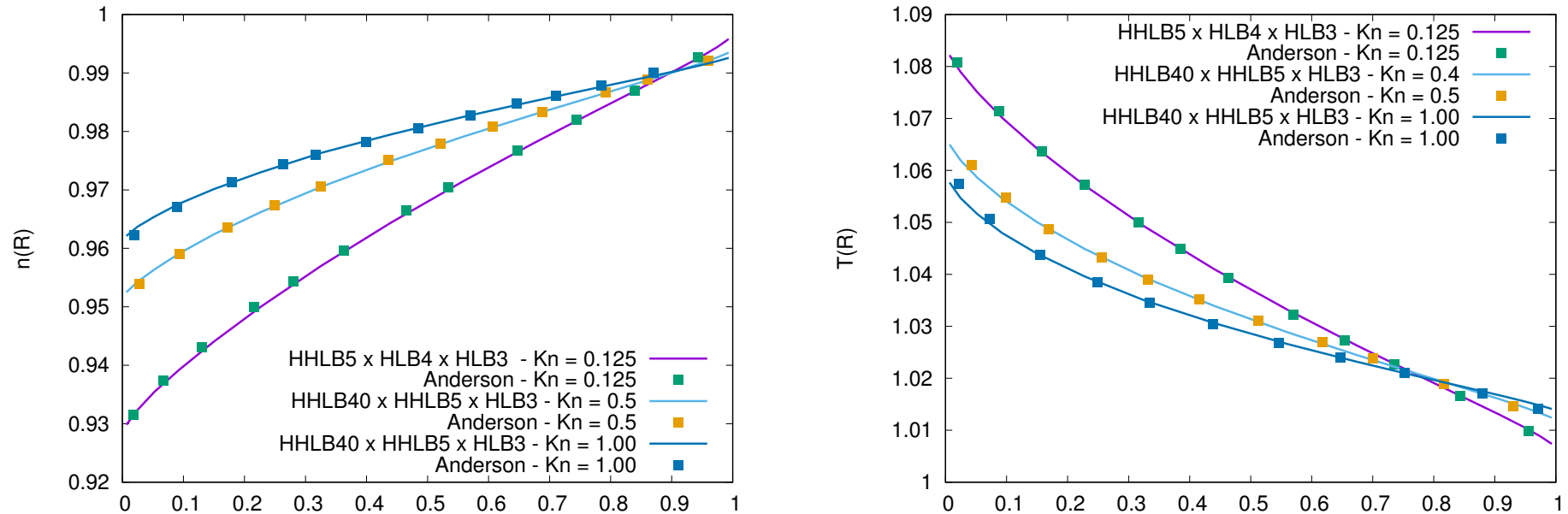


Figure 4: Heat transfer comparison with the study of Anderson⁹ for $\Delta T = 0.1$

⁹Donald G. M. Anderson, J. Plasma Physics (1967), vol. 1, part 2, pp. 255-265

Cylindrical Symmetry - transition regime

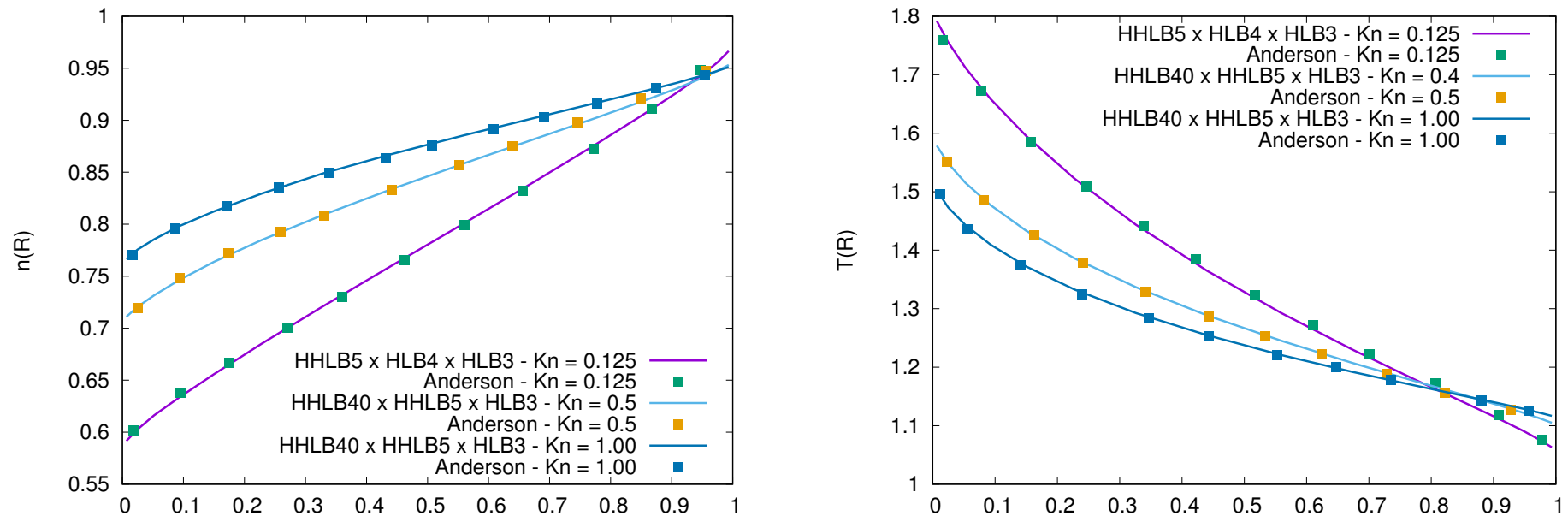


Figure 5: Heat transfer comparison with the study of Anderson¹⁰ for $\Delta T = 1.0$.

¹⁰Donald G. M. Anderson, J. Plasma Physics (1967), vol. 1, part 2, pp. 255-265

Cylindrical Symmetry - transition regime

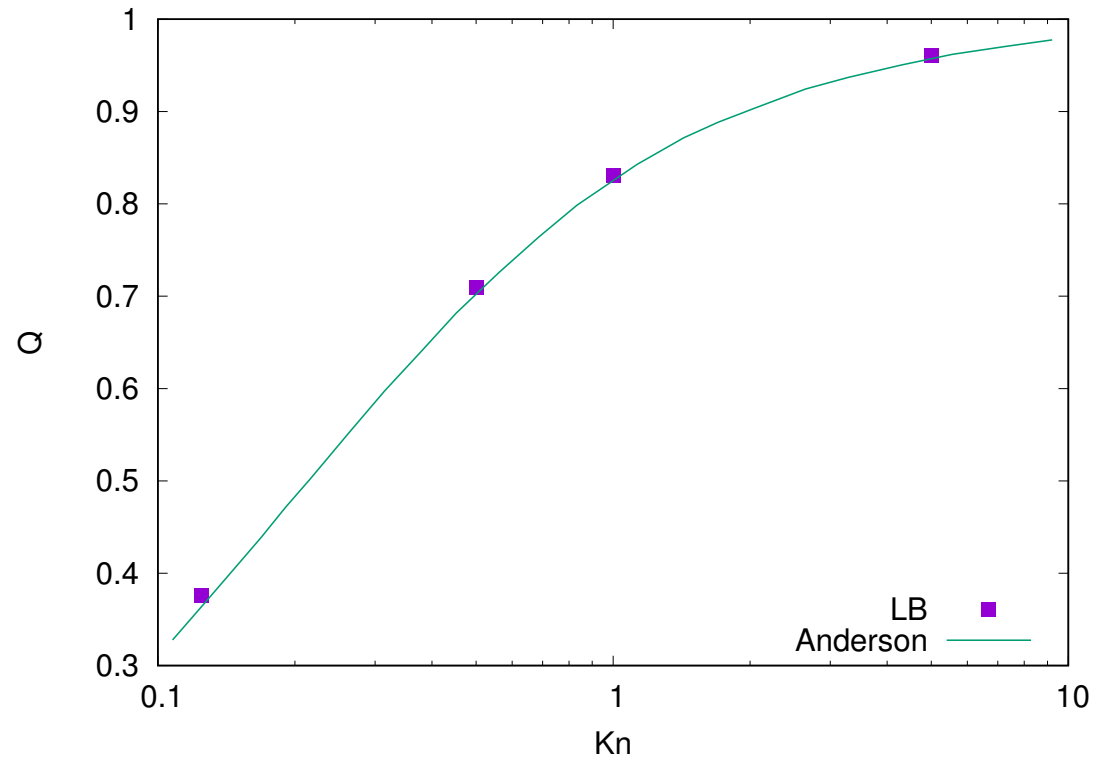


Figure 6: Q constant comparison with the study of Anderson¹¹.
 $Q = q(R) \cdot R$

¹¹Donald G. M. Anderson, J. Plasma Physics (1967), vol. 1, part 2, pp. 255-265

Spherical Symmetry - transition regime

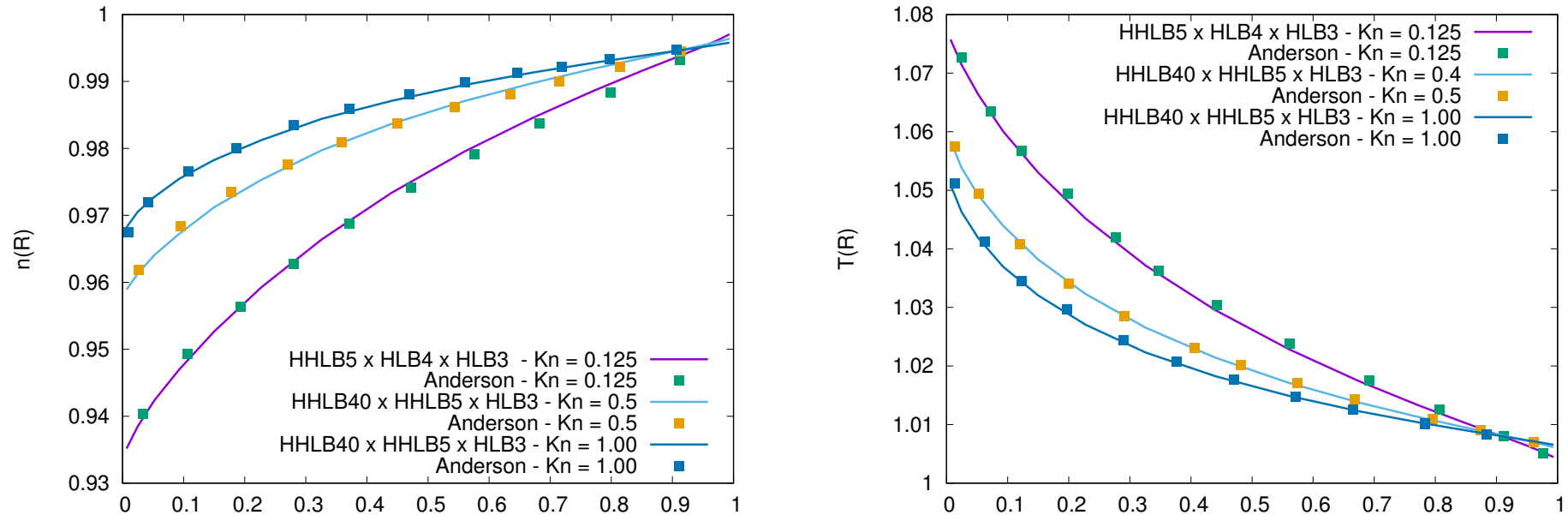


Figure 7: Heat transfer comparison with the study of Anderson¹² for $\Delta T = 0.1$.

¹²Donald G. M. Anderson, J. Plasma Physics (1967), vol. 1, part 2, pp. 255-265

Spherical Symmetry - transition regime

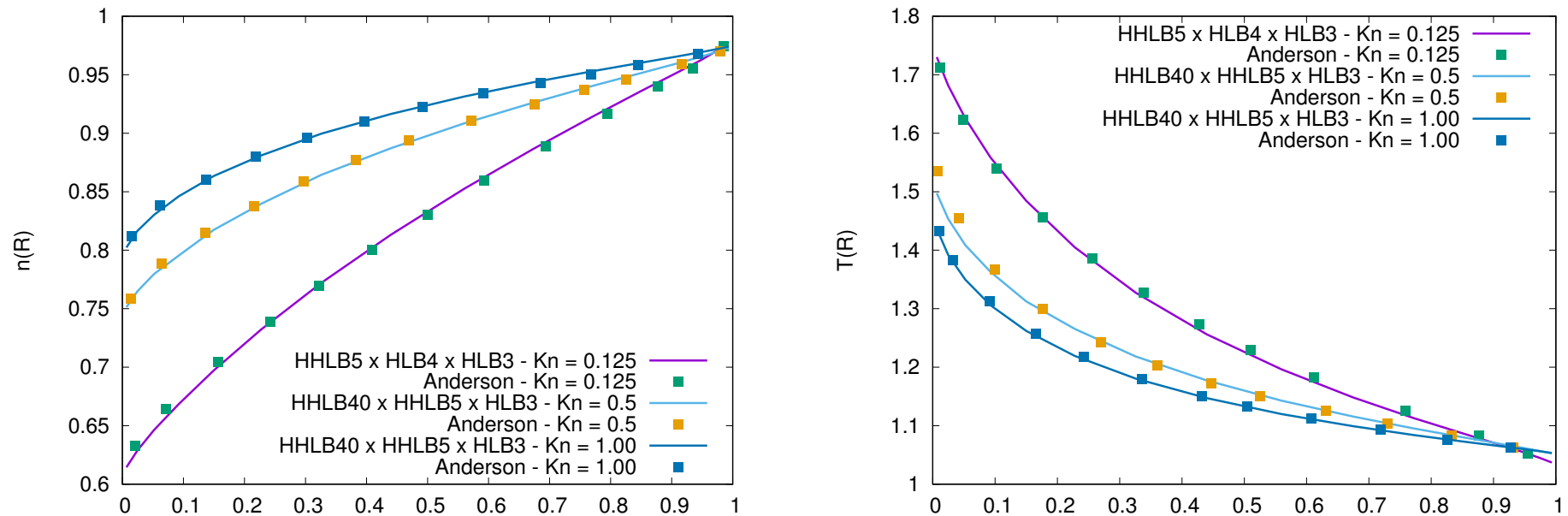


Figure 8: Heat transfer comparison with the study of Anderson¹³ for $\Delta T = 1.0$.

¹³Donald G. M. Anderson, J. Plasma Physics (1967), vol. 1, part 2, pp. 255-265

Spherical Symmetry - transition regime

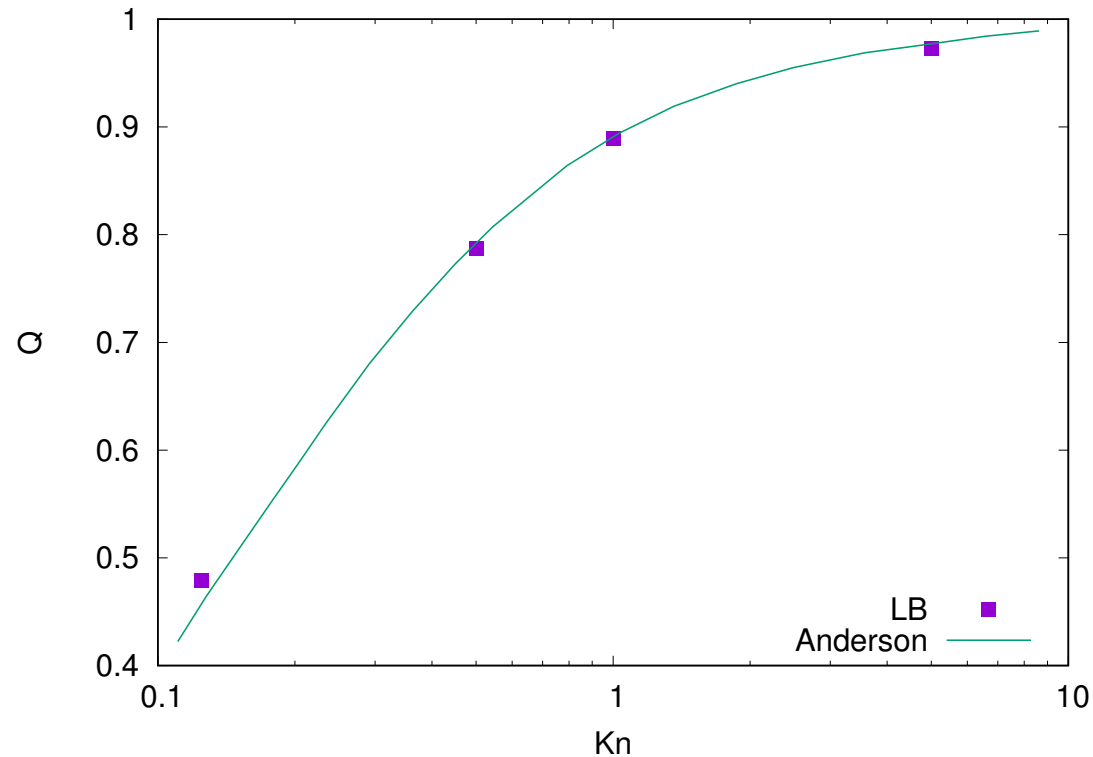
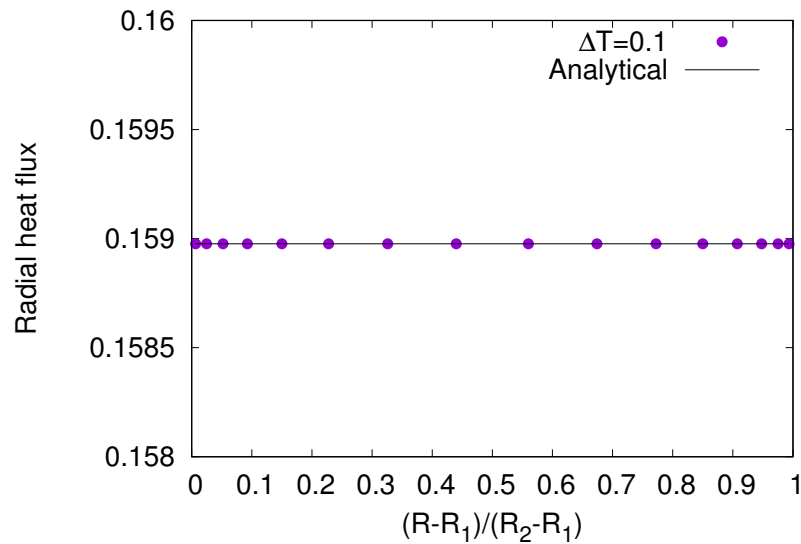
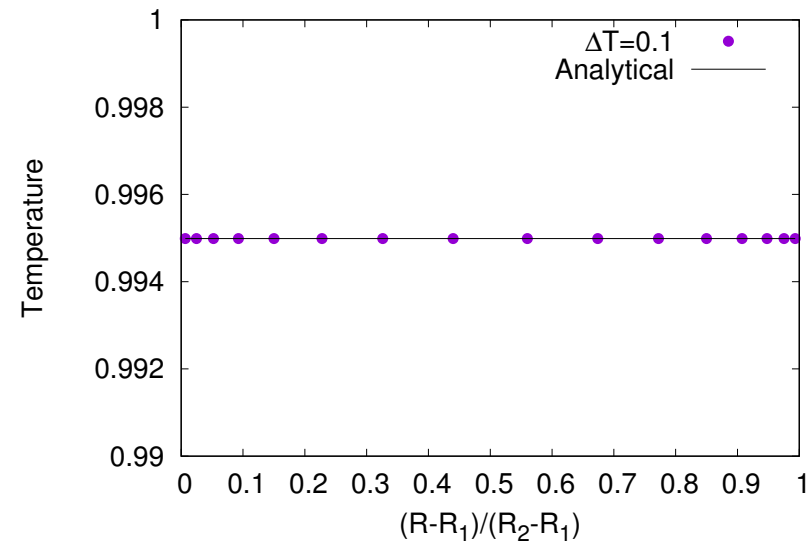
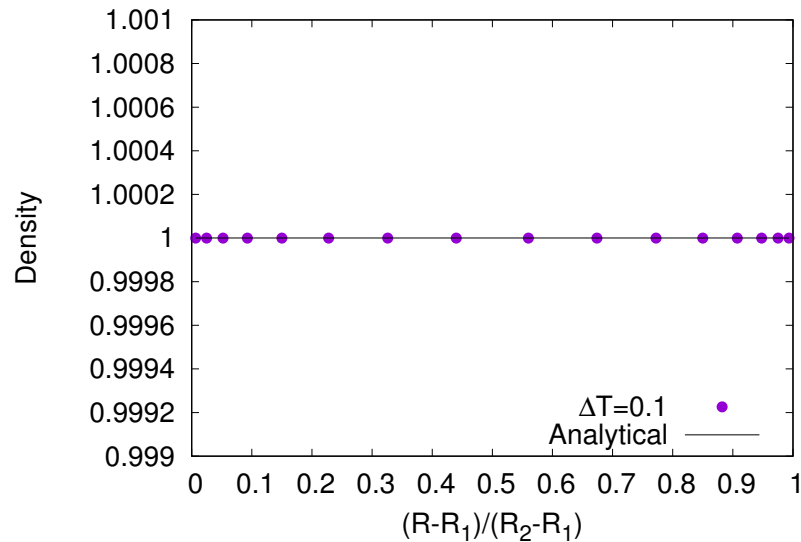


Figure 9: Q constant comparison with the study of Anderson¹⁴.
 $Q = q(R) \cdot R^2$

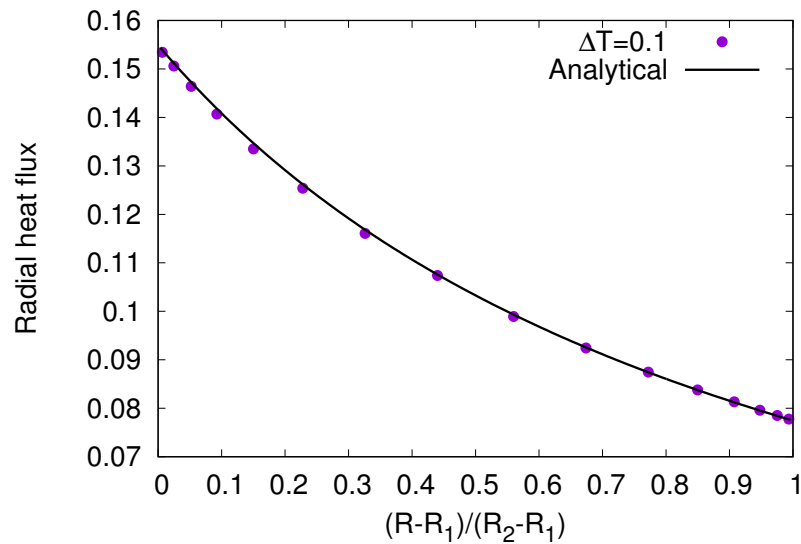
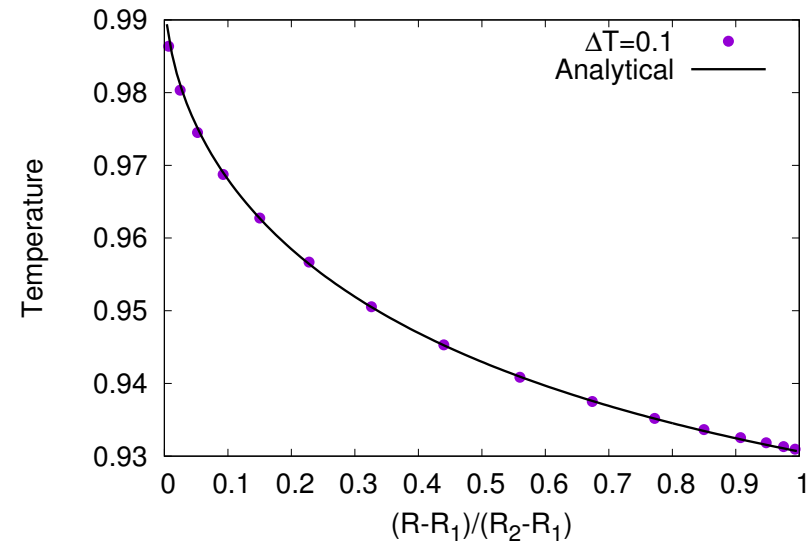
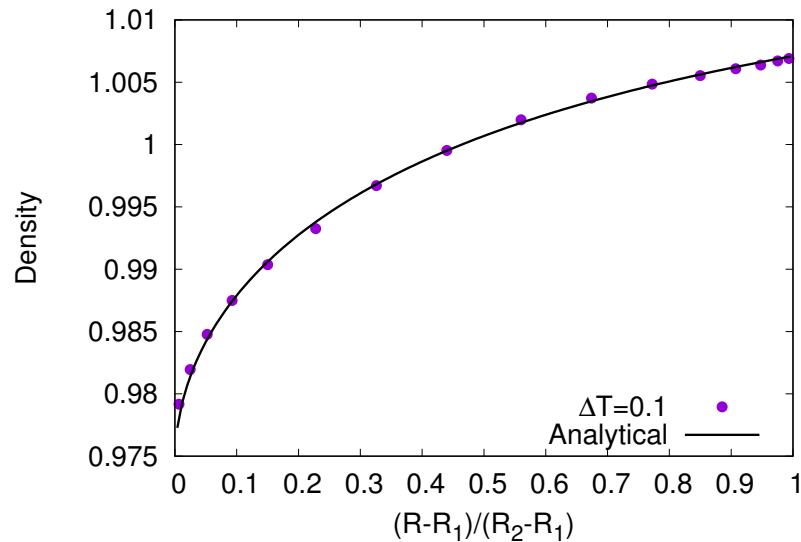
¹⁴Donald G. M. Anderson, J. Plasma Physics (1967), vol. 1, part 2, pp. 255-265

Parallel plates $Kn \rightarrow \infty$



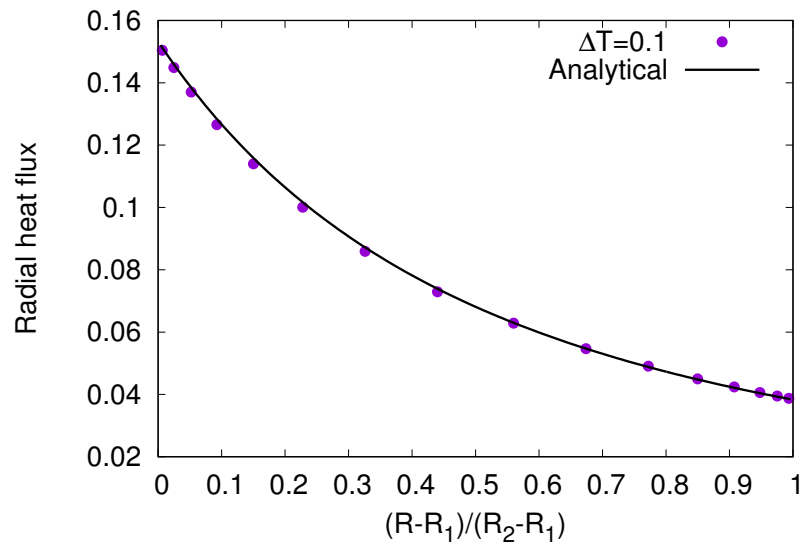
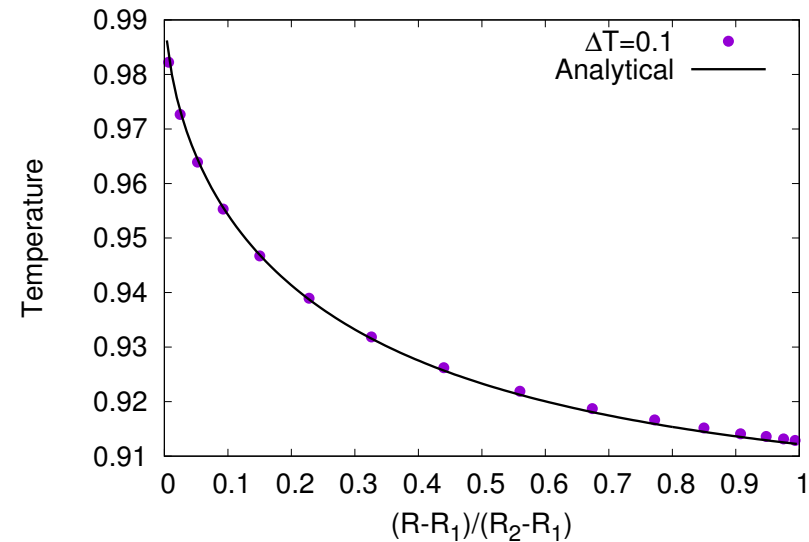
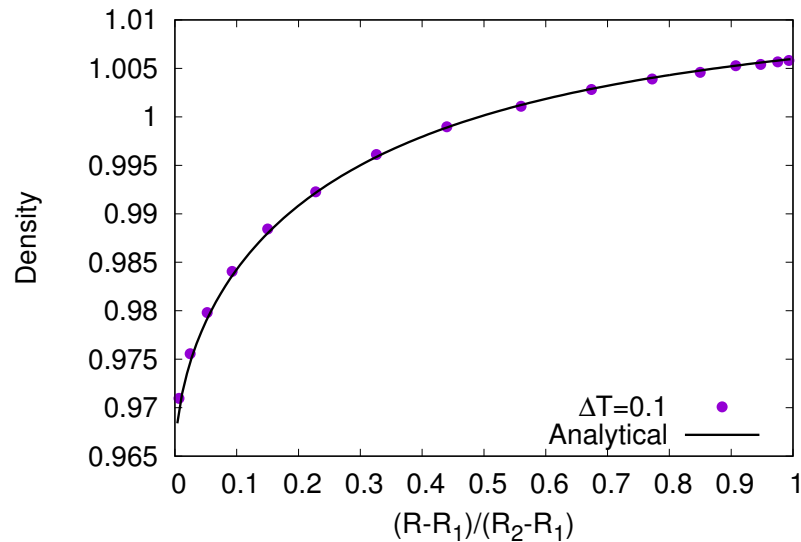
Profiles of number density, temperature for a wall temperature spread $\Delta T = 0.1$.

Cylindrical symmetry $Kn \rightarrow \infty$



Profiles of number density, temperature for a wall temperature spread $\Delta T = 0.1$.

Spherical symmetry $Kn \rightarrow \infty$



Profiles of number density, temperature for a wall temperature spread $\Delta T = 0.1$.

Conclusion

- We introduced the Boltzmann equation written with respect to orthogonal vielbeins.
- The vielbeins allow the decoupling between the momentum space and the coordinate space, i.e. $\mathbf{p}^2$ is coordinate-independent.
- The vielbein permits the momentum space degrees of freedom to be aligned according to the symmetries of the flow.
- We considered the problems of heat transfer between parallel plates, two coaxial cylinders and two concentric spheres which become one-dimensional in space since the vielbein allows the symmetry of the geometry to be transferred to the momentum space.
- Our models give accurate results throughout the whole range of Kn.

Thank you for your attention.

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