

Mixed quadrature lattice Boltzmann models for the simulation of the circular Couette flow using the vielbein formalism

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Outline

- Boltzmann equation with respect to arbitrary coordinates system
- Boltzmann equation with respect to orthonormal vielbein fields
- Gauss-Hermite quadrature
- Circular Couette flow: Shear flows between coaxial cylinders
 - Rigid rotation
 - Hydrodynamic, transition and ballistic flow regimes

Boltzmann equation

- Evolution equation of the one-particle distribution function f with respect to the Cartesian coordinates:

$$\frac{\partial f}{\partial t} + \frac{p^i}{m} \frac{\partial f}{\partial x^i} + F^i \frac{\partial f}{\partial p^i} = J[f]. \quad (1)$$

- Hydrodynamic moments of order N give macroscopic quantities:

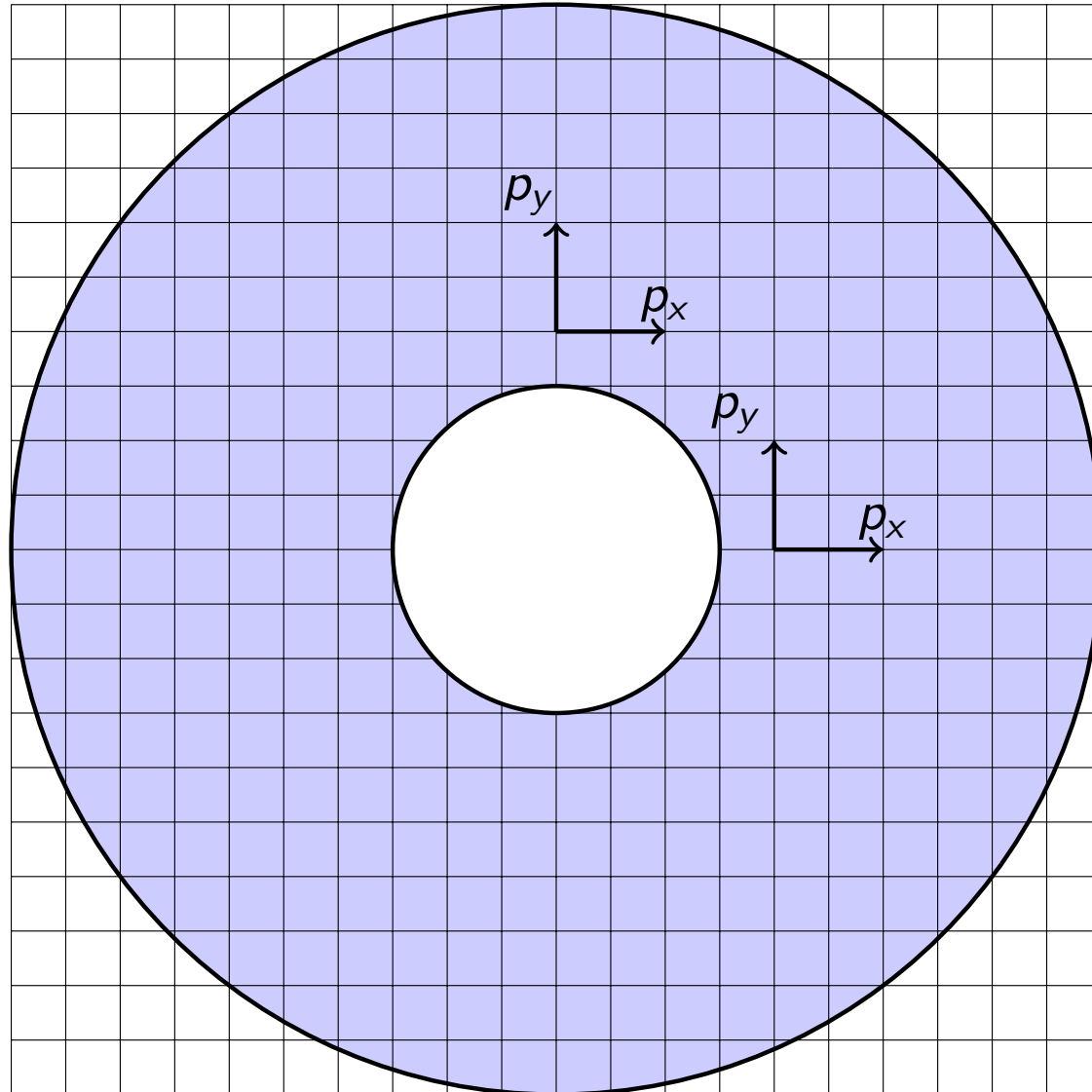
$$N=0 : \quad \text{number density:} \quad n = \int d^3 p f,$$

$$N=1 : \quad \text{velocity:} \quad \mathbf{u} = \frac{1}{nm} \int d^3 p f \mathbf{p},$$

$$N=2 : \quad \text{temperature:} \quad T = \frac{2}{3n} \int d^3 p f \frac{\xi^2}{2m}, \quad (\xi = \mathbf{p} - m\mathbf{u}),$$

$$N=3 : \quad \text{heat flux:} \quad \mathbf{q} = \frac{1}{2m^2} \int d^3 p f \xi^2 \xi.$$

Cartesian grid and momentum space decomposition along the Cartesian axes.



Boltzmann equation - arbitrary coordinates

- Consider a coordinate transformation $x^i \rightarrow \tilde{x}^{\tilde{i}}$, which induces a metric $\tilde{g}_{\tilde{i}\tilde{j}}$, as follows:

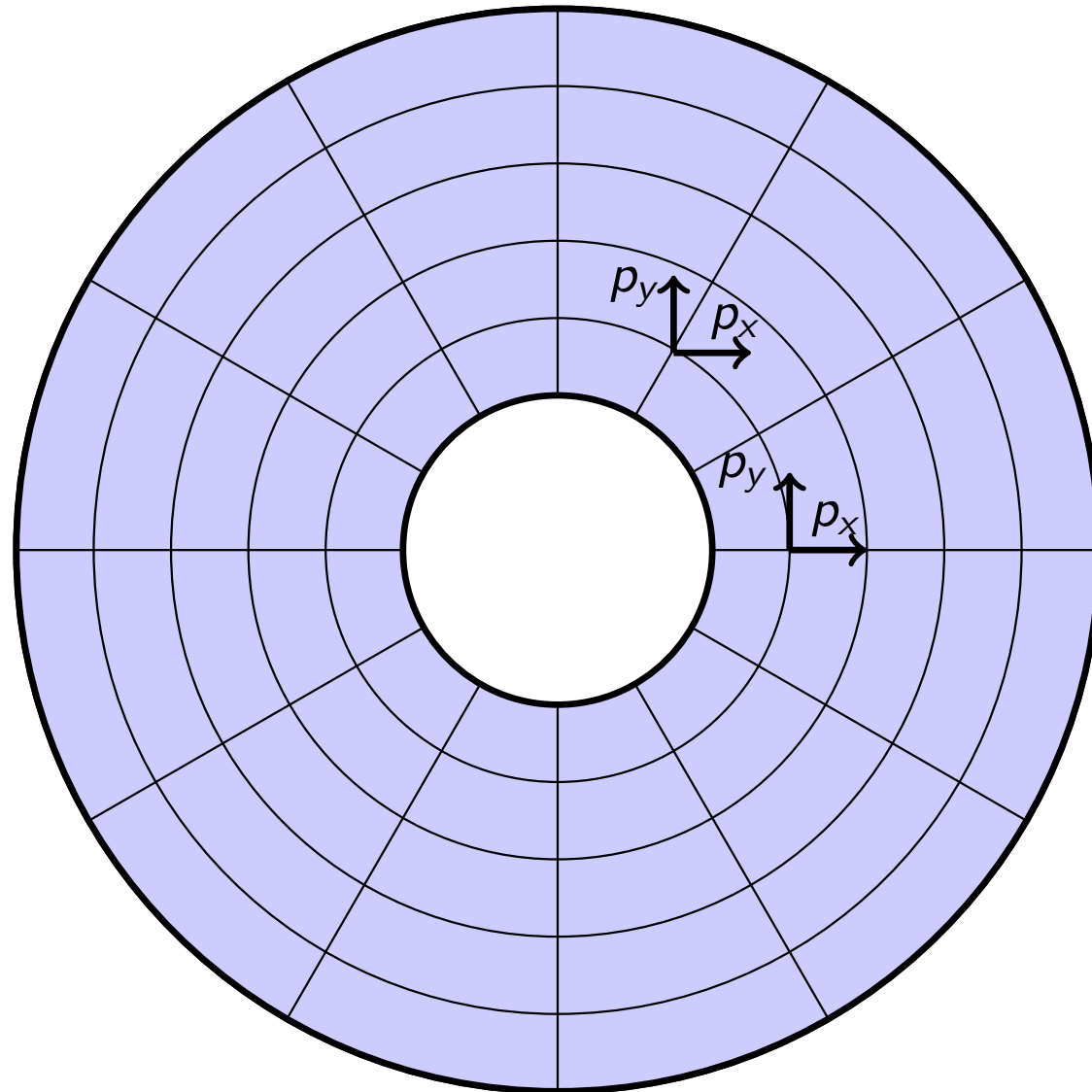
$$ds^2 = \delta_{ij} dx^i dx^j = \tilde{g}_{\tilde{i}\tilde{j}} d\tilde{x}^{\tilde{i}} d\tilde{x}^{\tilde{j}},$$

$$\tilde{g}_{\tilde{i}\tilde{j}} = \delta_{ij} \frac{\partial x^i}{\partial \tilde{x}^{\tilde{i}}} \frac{\partial x^j}{\partial \tilde{x}^{\tilde{j}}}.$$

- The Boltzmann equation with respect to the new spatial coordinates reads:

$$\frac{\partial f}{\partial t} + \frac{p^i}{m} \frac{\partial \tilde{x}^{\tilde{i}}}{\partial x^i} \frac{\partial f}{\partial \tilde{x}^{\tilde{i}}} + F^i \frac{\partial f}{\partial p^i} = J[f]. \quad (2)$$

Cylindrical grid and momentum space decomposition along the Cartesian axes



Boltzmann equation - orthonormal vielbein fields

- Furthermore, we note that:

$$p^{\tilde{i}} = p^i \frac{\partial x^{\tilde{i}}}{\partial x^i}, \quad F^{\tilde{i}} = F^i \frac{\partial x^{\tilde{i}}}{\partial x^i}, \quad \mathbf{p}^2 \equiv g_{\tilde{i}\tilde{j}} p^{\tilde{i}} p^{\tilde{j}}$$

- By introducing the triad vector frame and the associated one-form co-frame:

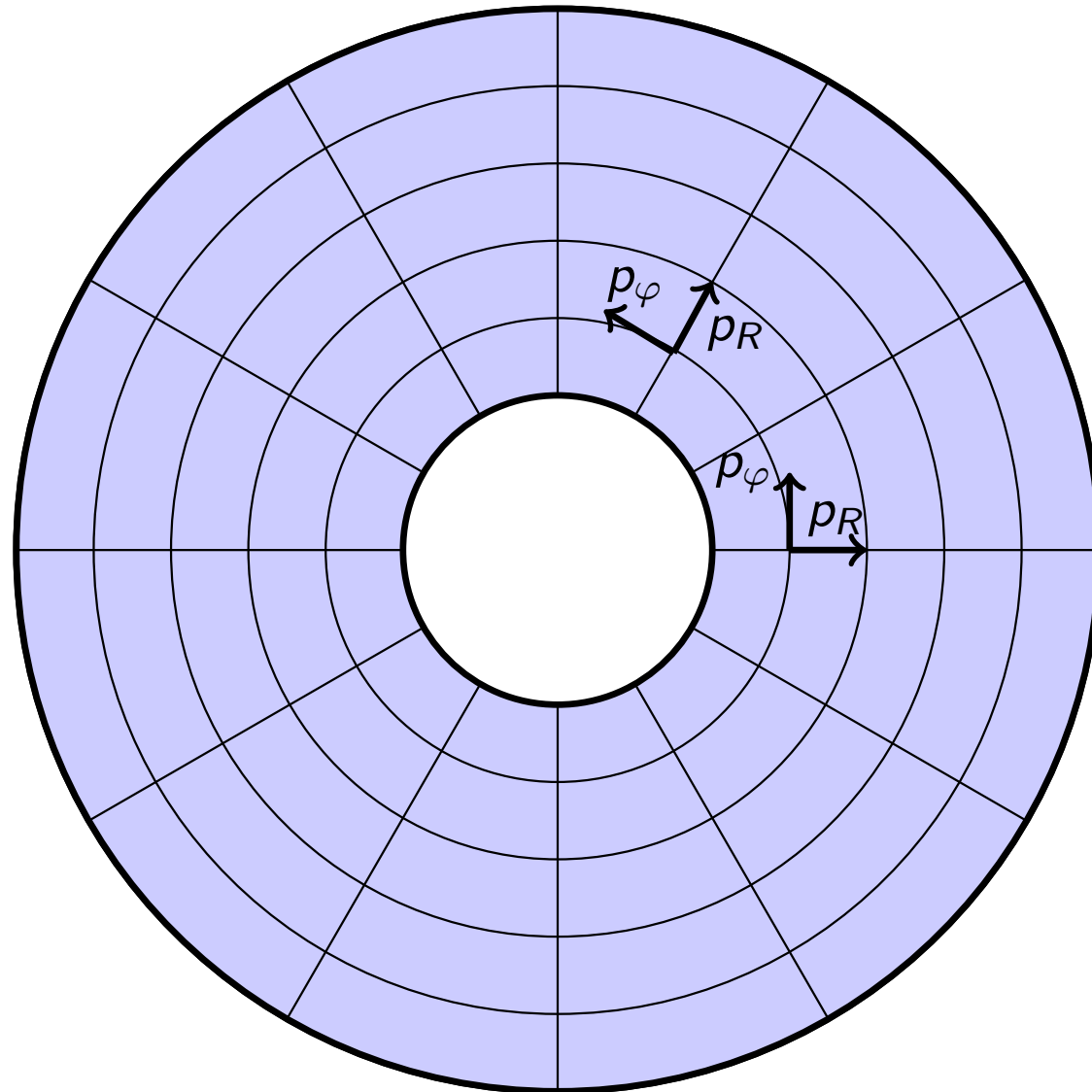
$$e_{\hat{a}} = e_{\hat{a}}^{\tilde{i}} \partial_{\tilde{i}}, \quad \omega^{\hat{a}} = \omega_{\tilde{i}}^{\hat{a}} dx^{\tilde{i}}, \quad g_{\tilde{i}\tilde{j}} dx^{\tilde{i}} dx^{\tilde{j}} = \delta_{\hat{a}\hat{b}} \omega^{\hat{a}} \omega^{\hat{b}}$$

the inner product $\mathbf{p}^2 \equiv \delta_{\hat{a}\hat{b}} p^{\hat{a}} p^{\hat{b}}$ is decoupled from the metric.

- The Boltzmann equation reads:

$$\frac{\partial f}{\partial t} + \frac{p^{\hat{a}}}{m} e_{\hat{a}}^{\tilde{i}} \frac{\partial f}{\partial x^{\tilde{i}}} + \left(F^{\hat{a}} - \frac{1}{m} \Gamma^{\hat{a}}_{\hat{b}\hat{c}} p^{\hat{b}} p^{\hat{c}} \right) \frac{\partial f}{\partial p^{\hat{a}}} = J[f], \quad (3)$$

Cylindrical grid and momentum space decomposition adapted to the curvilinear coordinates.



Cylindrical coordinates

- The line element in cylindrical coordinates and the associated triad are:

$$ds^2 = dR^2 + R^2 d\varphi^2 + dz^2, \quad e_{\hat{R}} = \partial_R, \quad e_{\hat{\varphi}} = R^{-1} \partial_{\varphi}, \quad e_{\hat{z}} = \partial_z.$$

- The Boltzmann equation when the flow is homogeneous w.r.t. φ and z reads:

$$\frac{\partial f}{\partial t} + \frac{2p^{\hat{R}}}{m} \frac{\partial(fR)}{\partial R^2} + \frac{1}{mR} \left[(p^{\hat{\varphi}})^2 \frac{\partial f}{\partial p^{\hat{R}}} - p^{\hat{R}} \frac{\partial(fp^{\hat{\varphi}})}{\partial p^{\hat{\varphi}}} \right] = -\frac{1}{\tau} (f - f^{(\text{eq})}). \quad (4)$$

- The advection term is implemented following Falle et al.¹

¹S. A. E. G. Falle and S. S. Komissarov, Mon. Not. R. Astron. Soc. **278**, 586-602 (1996).

Coordinates stretching

$$\text{Let } R(\eta) = R_{\text{in}} + (R_{\text{out}} - R_{\text{in}}) \left(\delta + \frac{A_0}{A} \tanh \eta \right), \quad A_0 = \max(\delta, 1 - \delta). \quad (5)$$

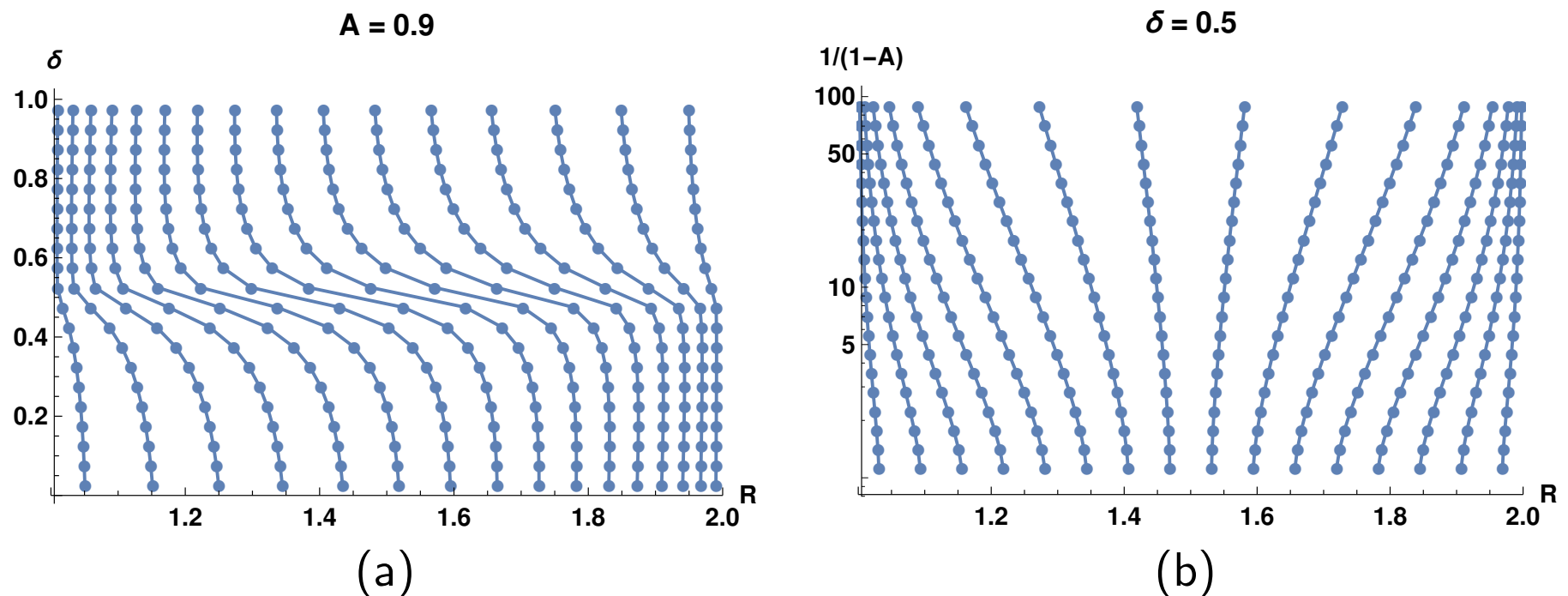


Figure: Effect of grid stretching on 16 points between $R_{\text{in}} = 1$ and $R_{\text{out}} = 2$.
(a) The parameter $\delta \in (0, 1)$ controls the positioning of the stretching centre.
(b) The parameter $A \in (0, 1)$ contains the amplitude of the stretching.
The points are equidistant in η .

Lattice Boltzmann - Gauss-Hermite quadratures

- The numerical models employed are mixed quadrature lattice Boltzmann². f and $f^{(eq)}$ are expanded with respect to Hermite(HLB) and Half-Range Hermite(HHLB) polynomials, e. g.(1D case):

$$f_i^{eq}(\mathbf{x}, t) = w_i \sum_{\ell=0}^N \frac{1}{\ell!} \mathbf{a}_{(\ell)}^{eq}(\mathbf{x}, t) \mathcal{H}^{(\ell)}(p_i)$$

- 3D model = 1D $\times$ 1D $\times$ 1D.
- We will denote such models by: HHLB(Q_R) $\times$ HLB(Q_φ) $\times$ HLB(Q_z).
- The moments of the distribution function are evaluated as:

$$\int d^3\hat{p} f p^{\hat{a}_1} \dots p^{\hat{a}_s} = \sum_{i=1}^{Q_R} \sum_{j=1}^{Q_\varphi} \sum_{k=1}^{Q_z} f_{ijk} \prod_{\ell=1}^s p_{ijk}^{\hat{a}_\ell}. \quad (6)$$

Here $Q_\alpha, \alpha \in \{R, \varphi, z\}$ represents the quadrature order.

²V.E. Ambrus and V. Sofonea, J. Comput. Phys. **316**, 760-788 (2016)

Force term

Boltzmann equation written for the discrete distributions f_{ijk} :

$$\frac{\partial f_{ijk}}{\partial t} + \frac{2p_i^{\hat{R}}}{m} \frac{\partial(f_{ijk}R)}{\partial R^2} + \frac{1}{mR} \left\{ (p_j^{\hat{\varphi}})^2 \left(\frac{\partial f}{\partial p^{\hat{R}}} \right)_{ijk} - p_i^{\hat{R}} \left[\frac{\partial(f p^{\hat{\varphi}})}{\partial p^{\hat{\varphi}}} \right]_{ijk} \right\} = -\frac{1}{\tau} (f_{ijk} - f_{ijk}^{(\text{eq})})$$

- We write the terms involving the derivative of f as follows³ :

$$\left(\frac{\partial f}{\partial p^{\hat{R}}} \right)_{ijk} = \sum_{i'=1}^{Q_R} \mathcal{F}_{i,i'}^R f_{i'jk},$$

- The matrix $\mathcal{F}_{k,j}^R$ has the following form:

$$\mathcal{F}_{k,j}^R = -w_k^H \sum_{\ell=0}^{Q-1} \frac{1}{\ell!} H_{\ell+1}(p_k) H_{\ell}(p_j)$$

³V. E. Ambruş, V. Sofonea, R. Fournier, and S. Blanco, *Implementation of the force term in half-range lattice Boltzmann models*, in preparation.

Lattice Boltzmann - Numerical scheme

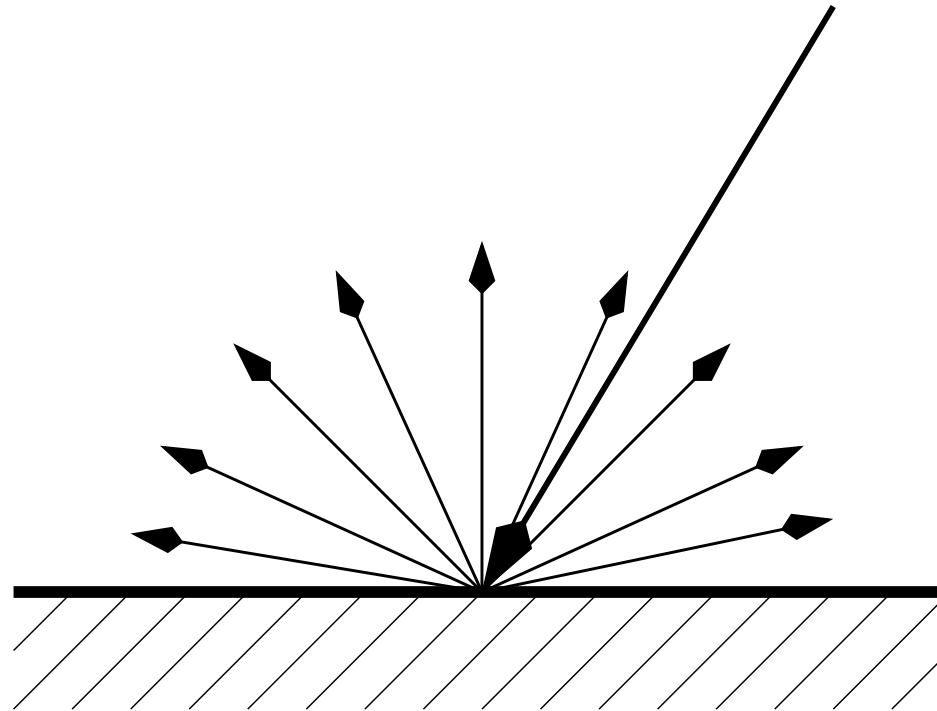
- Velocity vectors are given by the roots of the Hermite/Half-Range Hermite polynomials.
- The roots are irrational numbers for a quadrature order $Q > 2$ which implies a off-lattice velocity set.
- Time-stepping: TVD RK3⁴
- Advection: The fifth order WENO-5 scheme⁵.

⁴C.-W. Shu and S. Osher, J. Comput. Phys. 77, 439–471 (1988).

⁵G. S. Jiang and C. W. Shu, J. Comput. Phys. 126, 202 (1996).

Diffuse reflection boundary conditions

- Reflected particles carry some information that belongs to the wall.

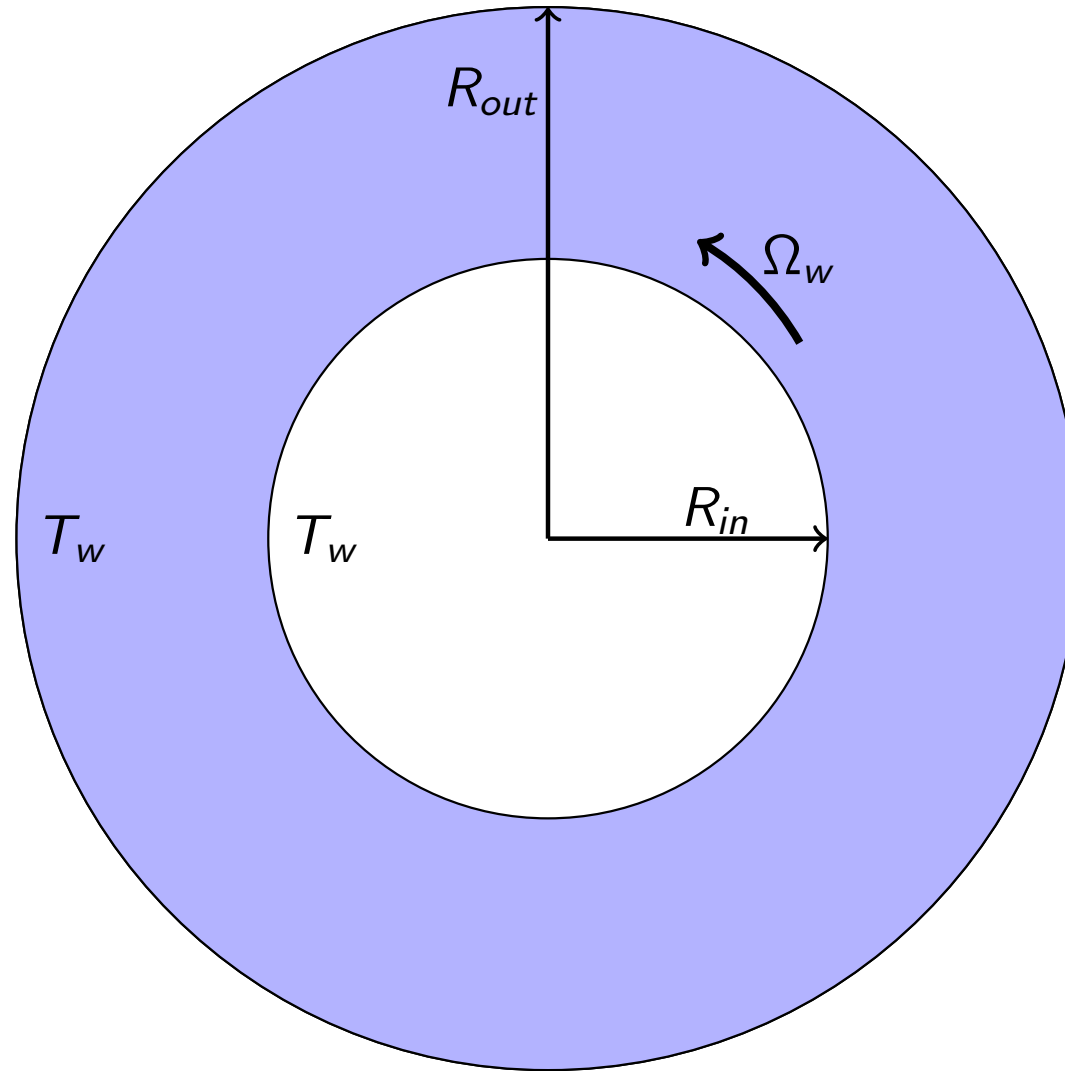


diffuse reflection

- The density n_w is fixed by imposing zero flux through the boundary:

$$\int_{\mathbf{p} \cdot \chi > 0} d^3 p f(\mathbf{p} \cdot \chi) = - \int_{\mathbf{p} \cdot \chi < 0} d^3 p f^{(\text{eq})}(\mathbf{p} \cdot \chi).$$

Circular Couette flow



Knudsen number $Kn = \lambda/L$.

Rigid rotation

- Angular speed $\Omega_{\text{in}} = \Omega_{\text{out}} = \Omega_w$, $T_{\text{in}} = T_{\text{out}} = T_w$, the analytic solution of the Boltzmann equation reads:

$$f(R) = \frac{n(R)}{(2\pi m T_w)^{3/2}} \exp \left[-\frac{p_{\hat{R}}^2 + (p_{\hat{\phi}} - \Omega R)^2 + p_{\hat{z}}^2}{2m T_w} \right], \quad (7)$$

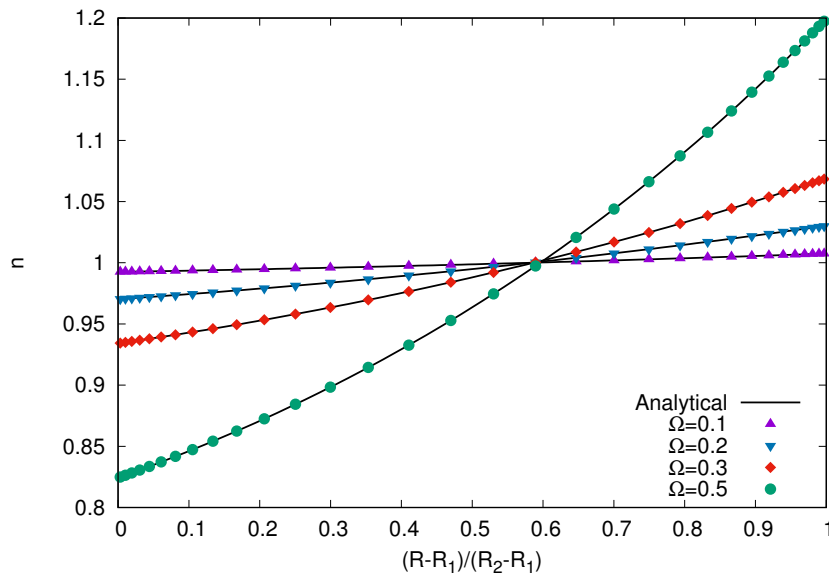
where $n(R)$ is given by ⁶:

$$n(R) = \frac{N}{H} \frac{m \Omega^2}{4\pi T_w} \frac{\exp \left[\frac{m \Omega^2}{4 T_w} (2R^2 - R_1^2 - R_2^2) \right]}{\sinh \left[\frac{m \Omega^2}{4 T_w} (R_2^2 - R_1^2) \right]}. \quad (8)$$

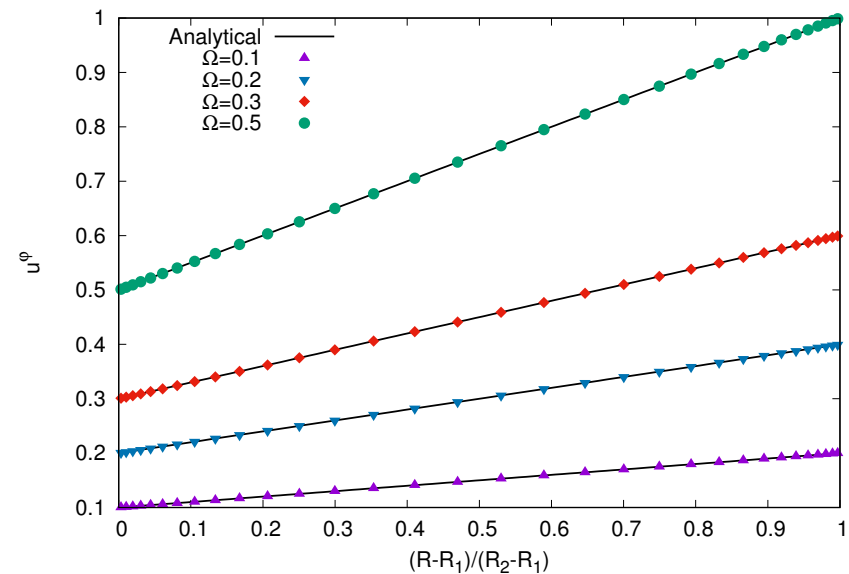
- Eq. (7) satisfies the Boltzmann equation for all values of the relaxation time.

⁶L. M. G. Cumin, G. M. Kremer, and F. Sharipov, Math. Mod. Meth. App. S. **12**, 445–459 (2002).

Rigid rotation



(a)



(b)

Figure: Comparison of simulation results with analytic solutions for results:
(a) Density profile ;
(b) Azimuthal velocity;
obtained using the $\text{HLB}(4) \times \text{HLB}(4) \times \text{HLB}(2)$ models and $N_R = 32$ nodes.

Hydrodynamic flow regime - $Kn \rightarrow 0$

- Number density is evaluated by numerically solving:

$$\partial_R \ln P = \frac{(u^{\hat{\varphi}})^2}{RT}. \quad (9)$$

where $n = P/T$ and by using the constraint $2\pi \int_{R_{\text{in}}}^{R_{\text{out}}} nRdR = N_{\text{tot}}$.

- Azimuthal velocity:

$$u^{\hat{\varphi}} = R^{-1} \frac{\Omega_{\text{in}}}{R_{\text{in}}^{-2} - R_{\text{out}}^{-2}} - R \frac{\Omega_{\text{in}} R_{\text{in}}^2}{R_{\text{out}}^2 - R_{\text{in}}^2}, \quad (10)$$

- Temperature:

$$T = T_w + \frac{\eta}{\kappa} \frac{\Omega_{\text{in}}^2}{R_{\text{in}}^{-2} - R_{\text{out}}^{-2}} \times \left(\frac{R_{\text{in}}^{-2} - R^{-2}}{R_{\text{in}}^{-2} - R_{\text{out}}^{-2}} - \frac{\ln(R/R_{\text{in}})}{\ln(R_{\text{out}}/R_{\text{in}})} \right) \quad (11)$$

- Radial heat flux:

$$q^{\hat{R}} = -\frac{\eta}{R} \frac{\Omega_{\text{in}}^2}{R_{\text{in}}^{-2} - R_{\text{out}}^{-2}} \times \left[\frac{2R^{-2}}{R_{\text{in}}^{-2} - R_{\text{out}}^{-2}} - \frac{1}{\ln(R_{\text{out}}/R_{\text{in}})} \right]. \quad (12)$$

Low Mach flows

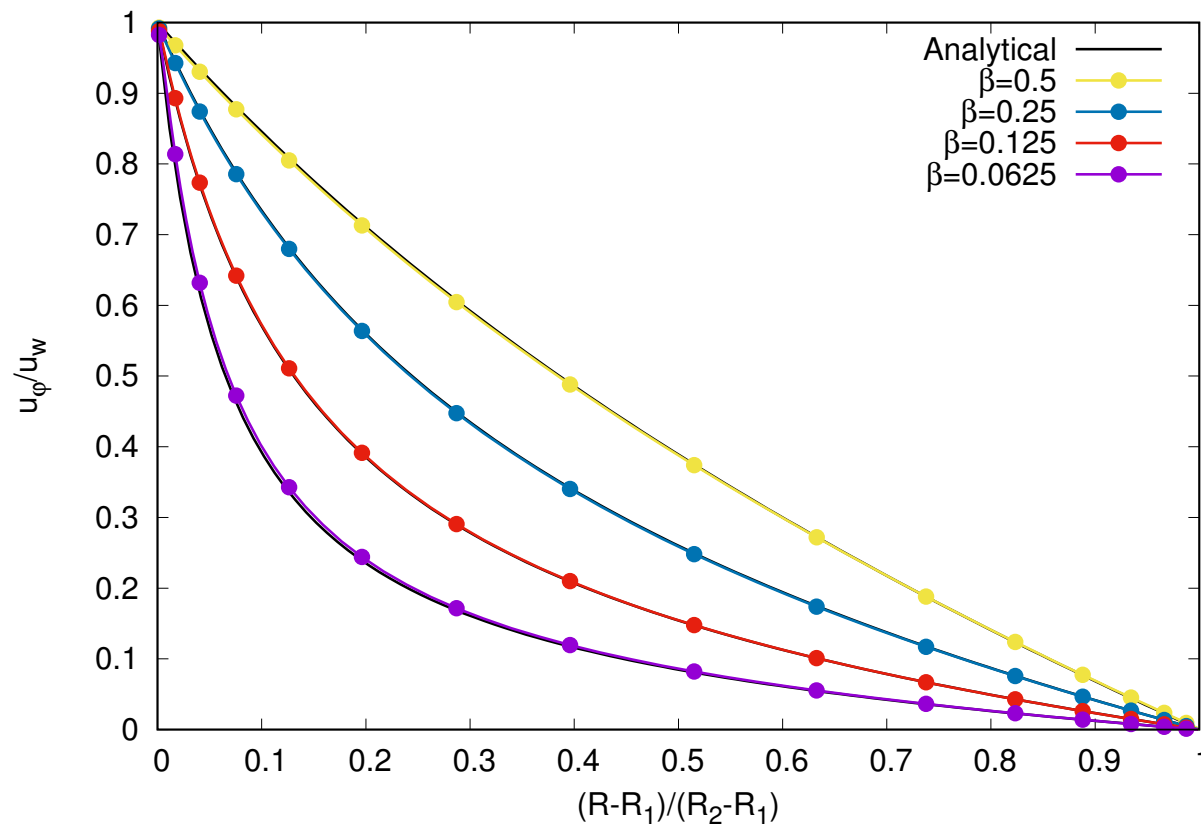


Figure: $u^\varphi(R)/u_w$ profile, where $u^\varphi = \Omega R$, $\Omega_{\text{in}} = 0.01$, $\beta = R_{\text{in}}/R_{\text{out}}$. Numerical results obtained using $\text{HLB}(3) \times \text{HLB}(3) \times \text{HLB}(2)$ models and $N_R = 64$ nodes.

Non-negligible Mach flows

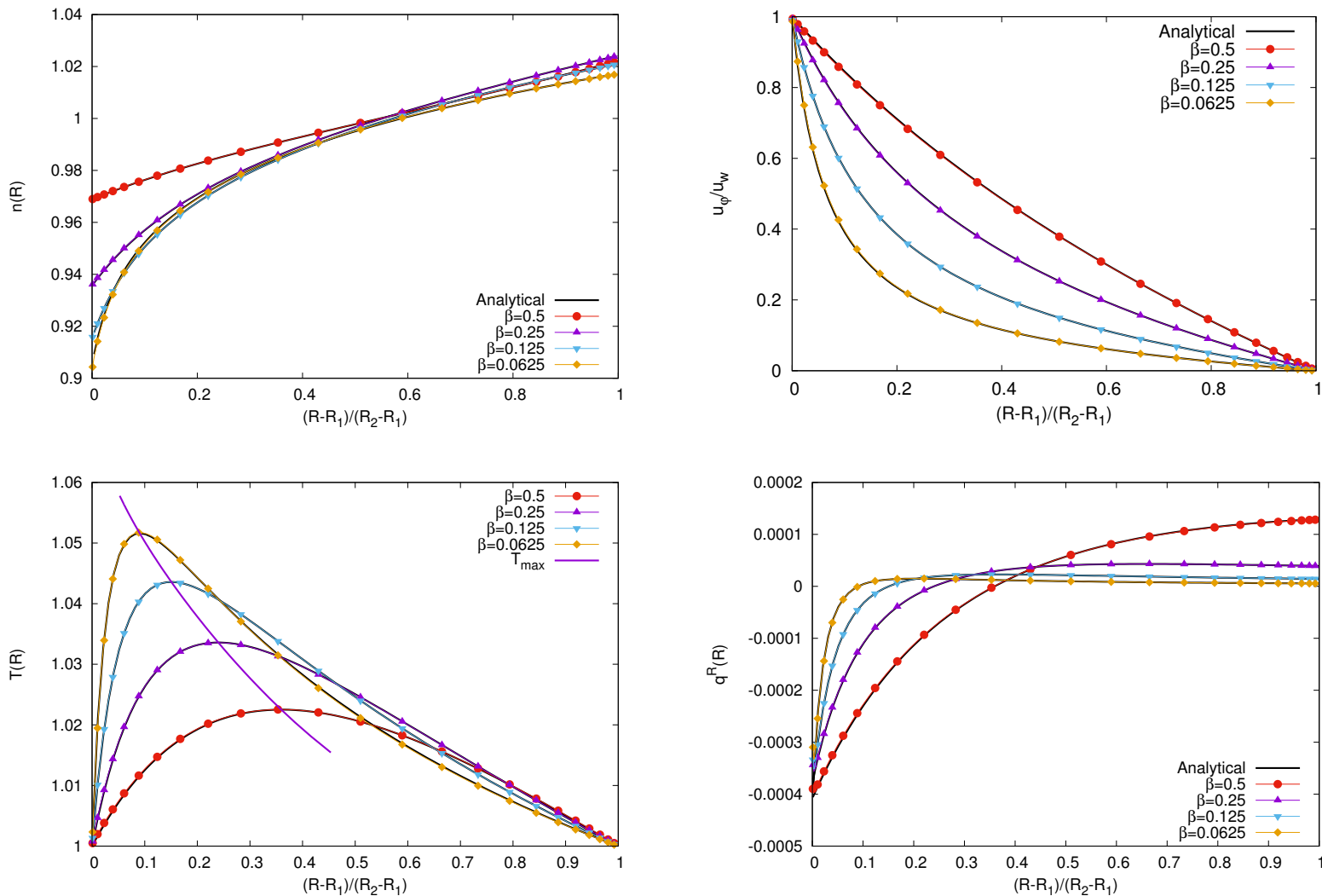


Figure: Comparison between the numerical and analytic results for the profiles of (a) $n(R)$; (b) $u^\phi(R)/u_w$; (c) $T(R)$; (d) $q^{\hat{R}}(R)$. $\beta = R_{in}/R_{out}$, $\Omega_{in} = 0.5$. Numerical results obtained using $HLB(5) \times HLB(5) \times HLB(3)$ models and $N_R = 96$ nodes.

Radial heat flux

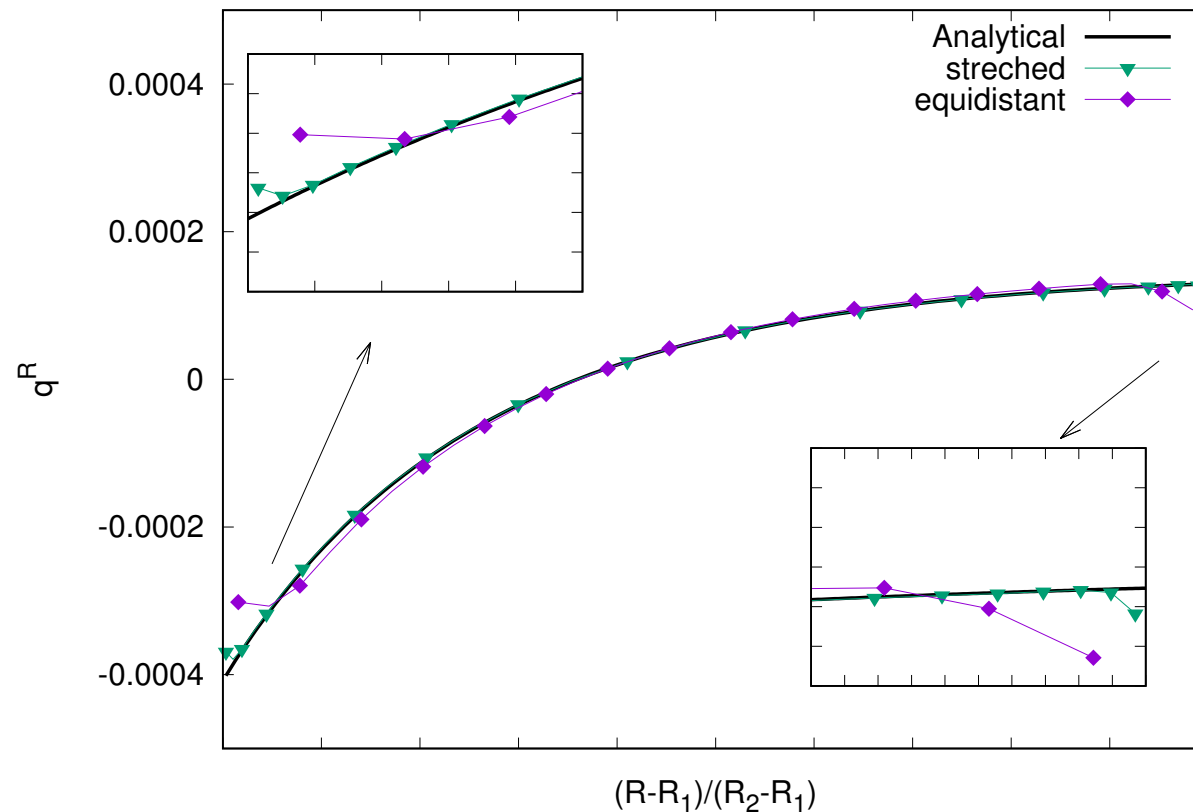
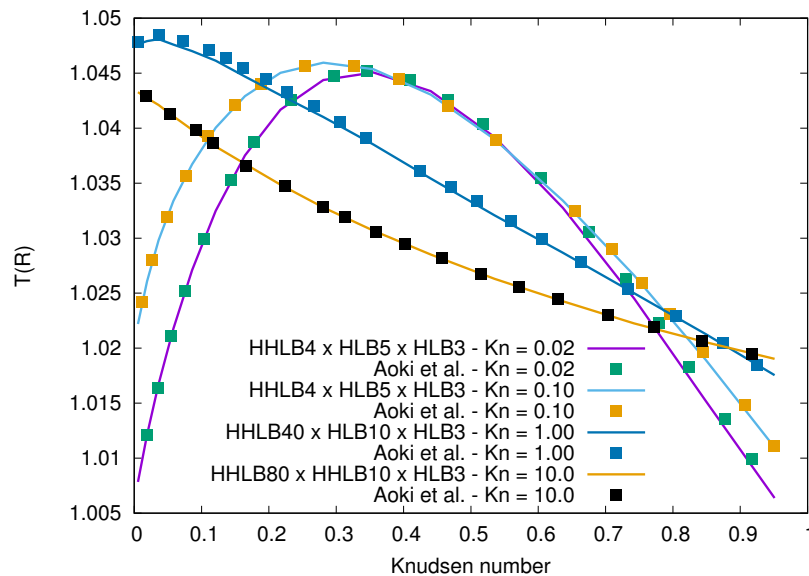
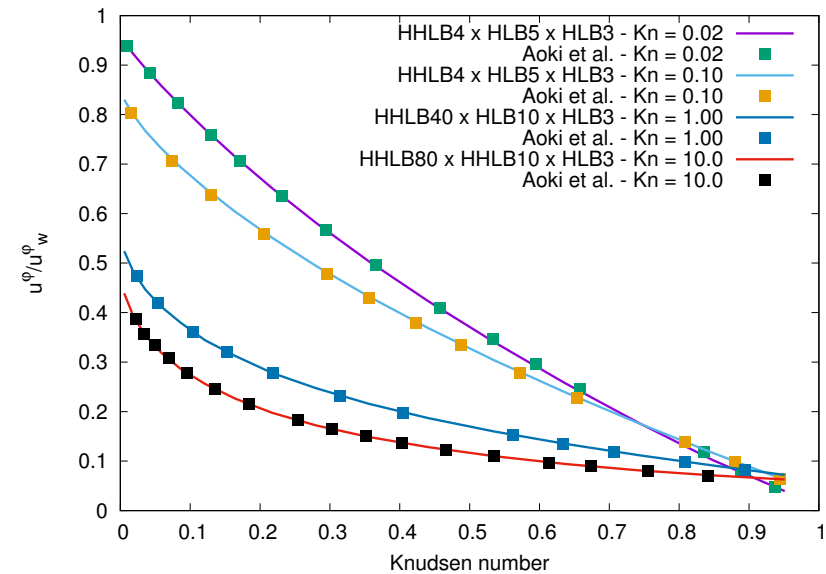
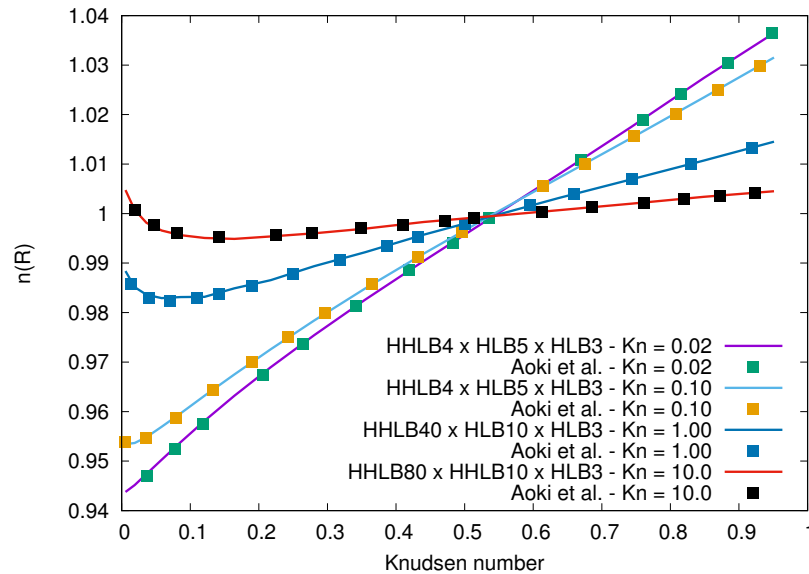


Figure: Comparison stretched and equidistant spatial discretisation with the same number of lattice nodes $N_R = 32$.

Transition flow regime



Comparison between our simulation results and those reported by Aoki et al.⁵: $n(R)$; $T(R)$; $u^\phi(R)/u_w^\phi$, $\Omega_{in} = 0.5\sqrt{2}$ and $N_R = 16$ nodes.

⁶K. Aoki, H. Yoshida, T. Nakanishi, and A. L. Garcia, Phys. Rev. E 68, 016302 (2003).

Free molecular flow regime - $Kn \rightarrow \infty$

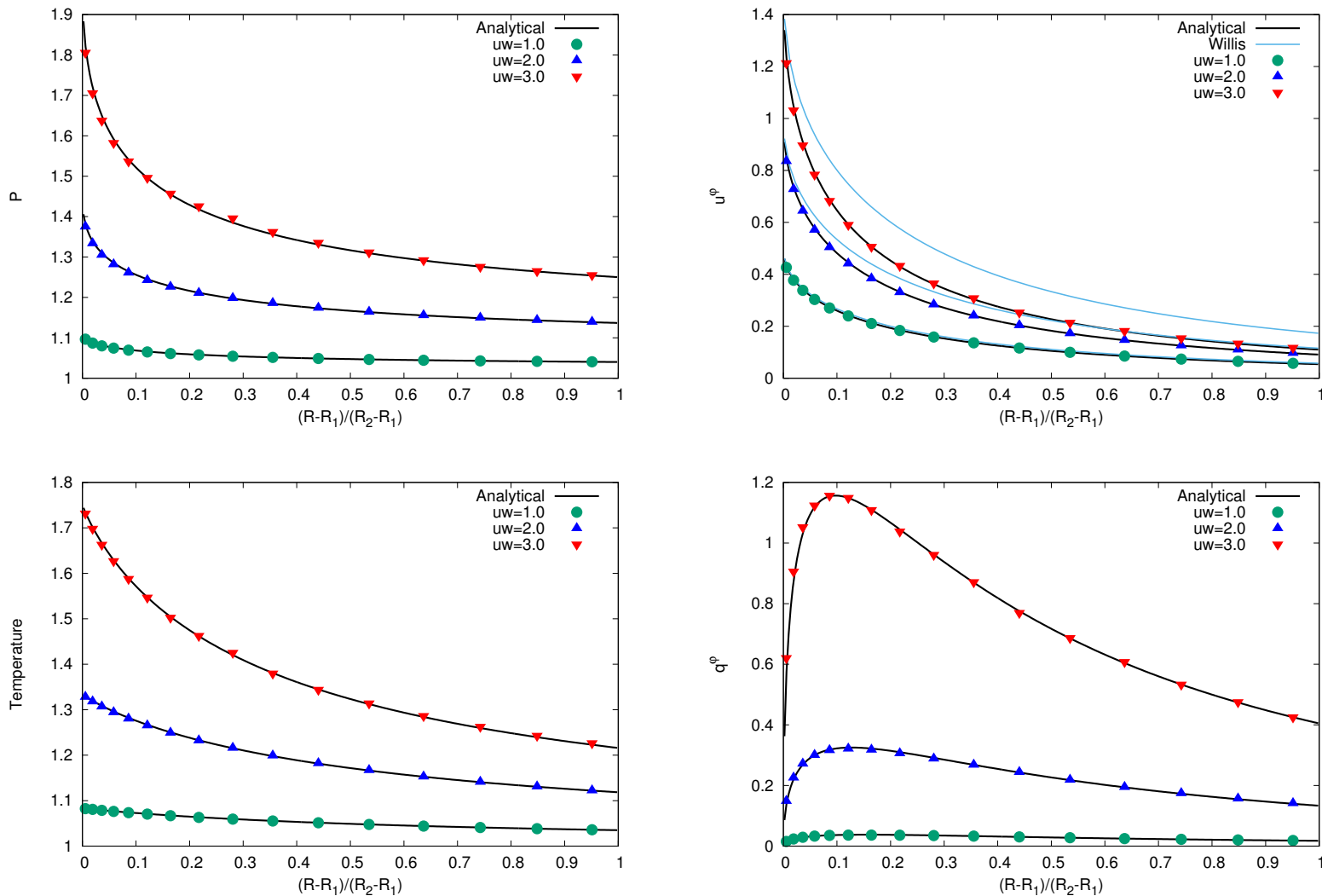


Figure: Comparison between our numerical results and the analytic predictions in the ballistic regime. (a) $P = n \cdot T$; (b) u^ϕ ; (c) T ; (d) q^ϕ . The HHLB(200) × HHLB(10) × HLB(3) model and $N_R = 16$ nodes. The analytic solution for u^ϕ reported by Willis⁸ is shown in (b) alongside our analytic expressions.

Conclusion

- We introduced the Boltzmann equation written with respect to orthogonal vielbeins.
- The vielbeins allow the decoupling between the momentum space and the coordinate space, i.e. $\mathbf{p}^2$ is coordinate-independent.
- The vielbein permits the momentum space degrees of freedom to be aligned according to the symmetries of the flow.
- We considered the shear flow between two coaxial cylinders(circular Couette flow) which becomes one-dimensional in space since the vielbein allows the symmetry of the geometry to be transferred to the momentum space.
- Our models give accurate results throughout the whole range of Kn.

Thank you for your attention.

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