

# LATTICE BOLTZMANN METHOD FOR MODELLING BIOPRINTED TISSUES

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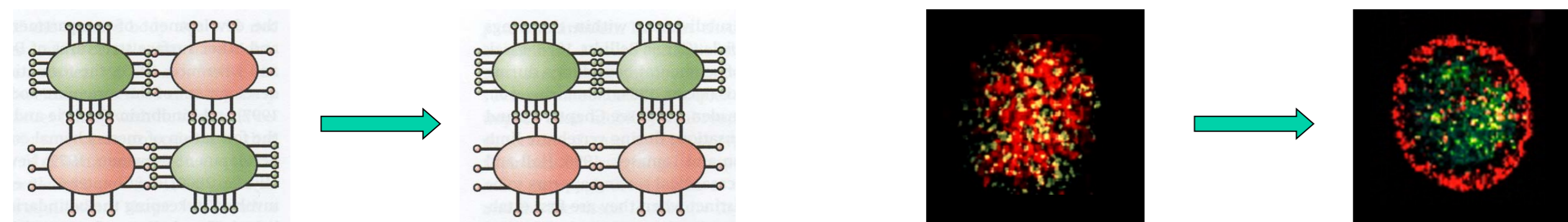
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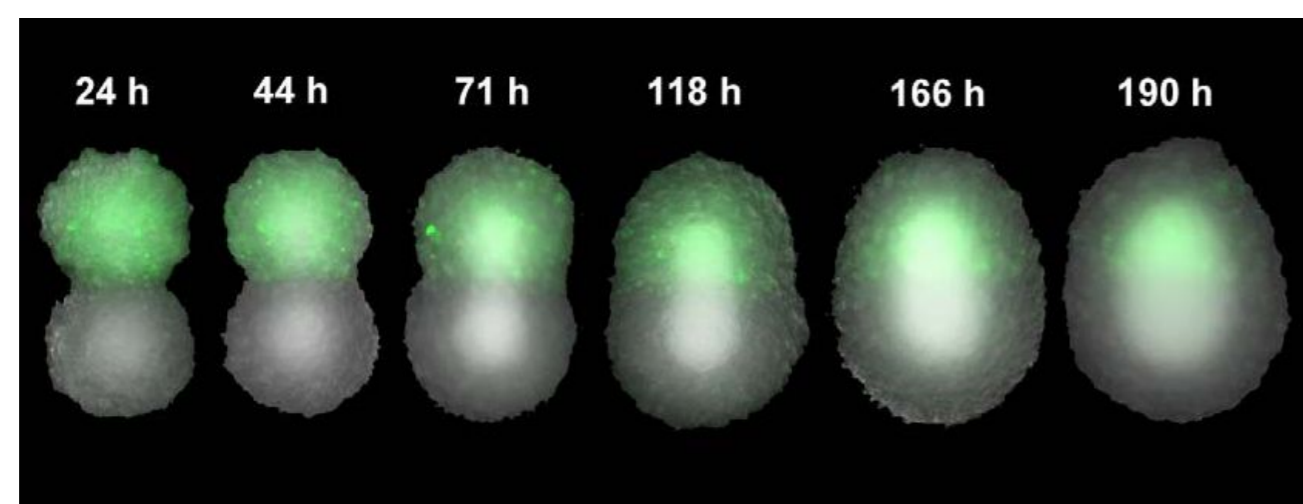
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## Differential Adhesion Hypothesis (DAH)<sup>1</sup>: cells seek partners to interact with

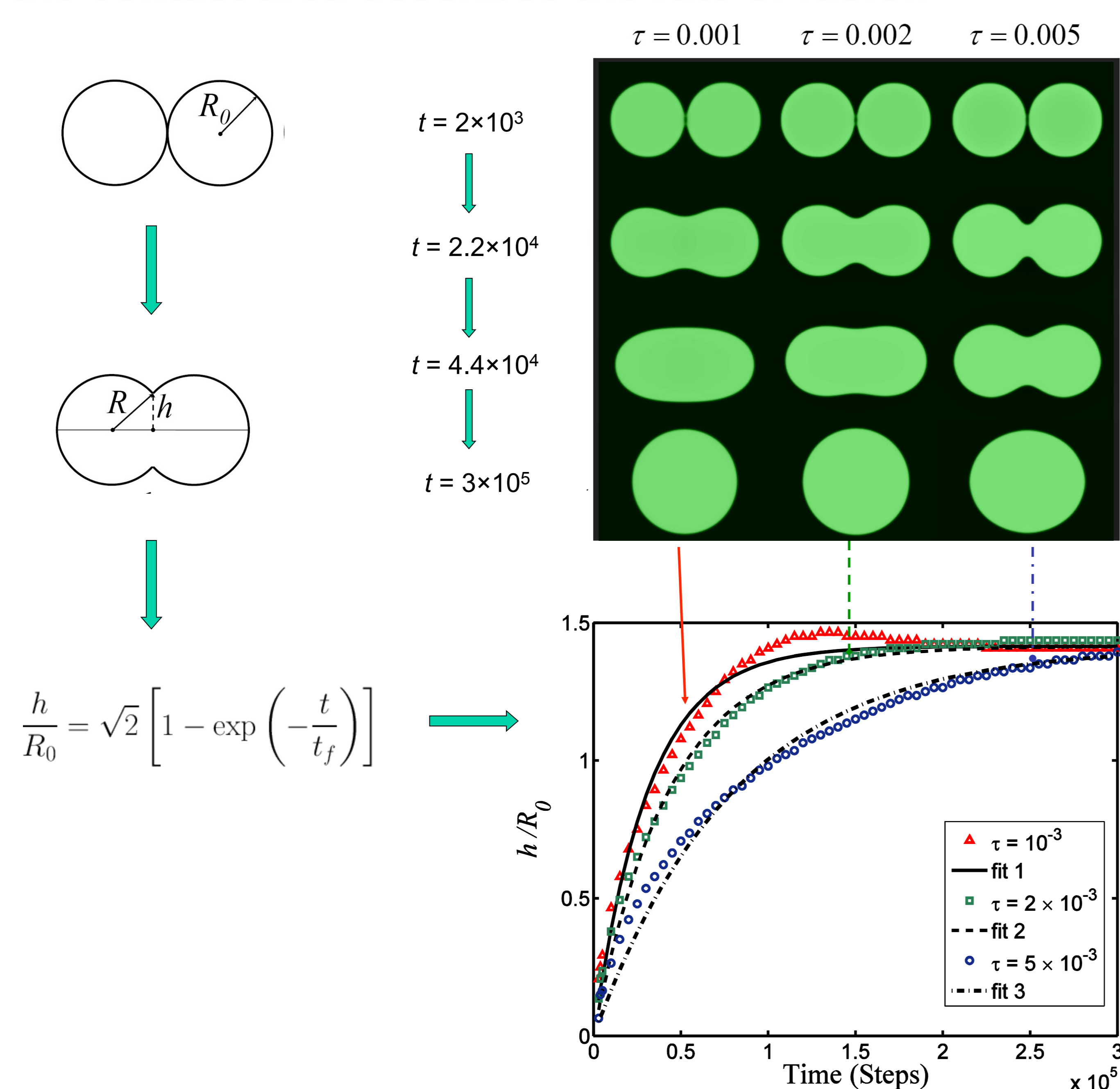


Tissue fusion is essential in developmental biology and tissue engineering

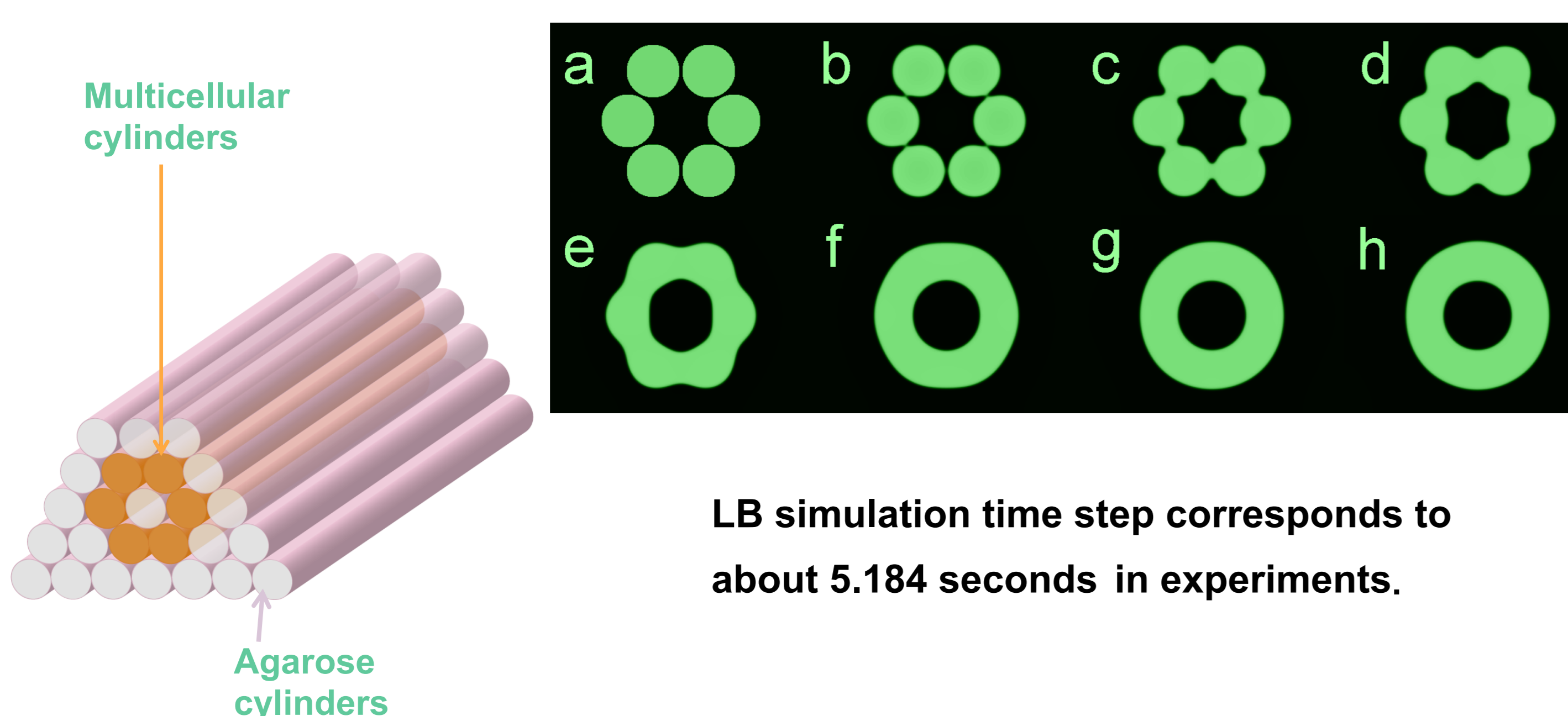


In vitro, aggregates of Chinese Hamster Ovary (CHO) cells fuse<sup>2</sup>.

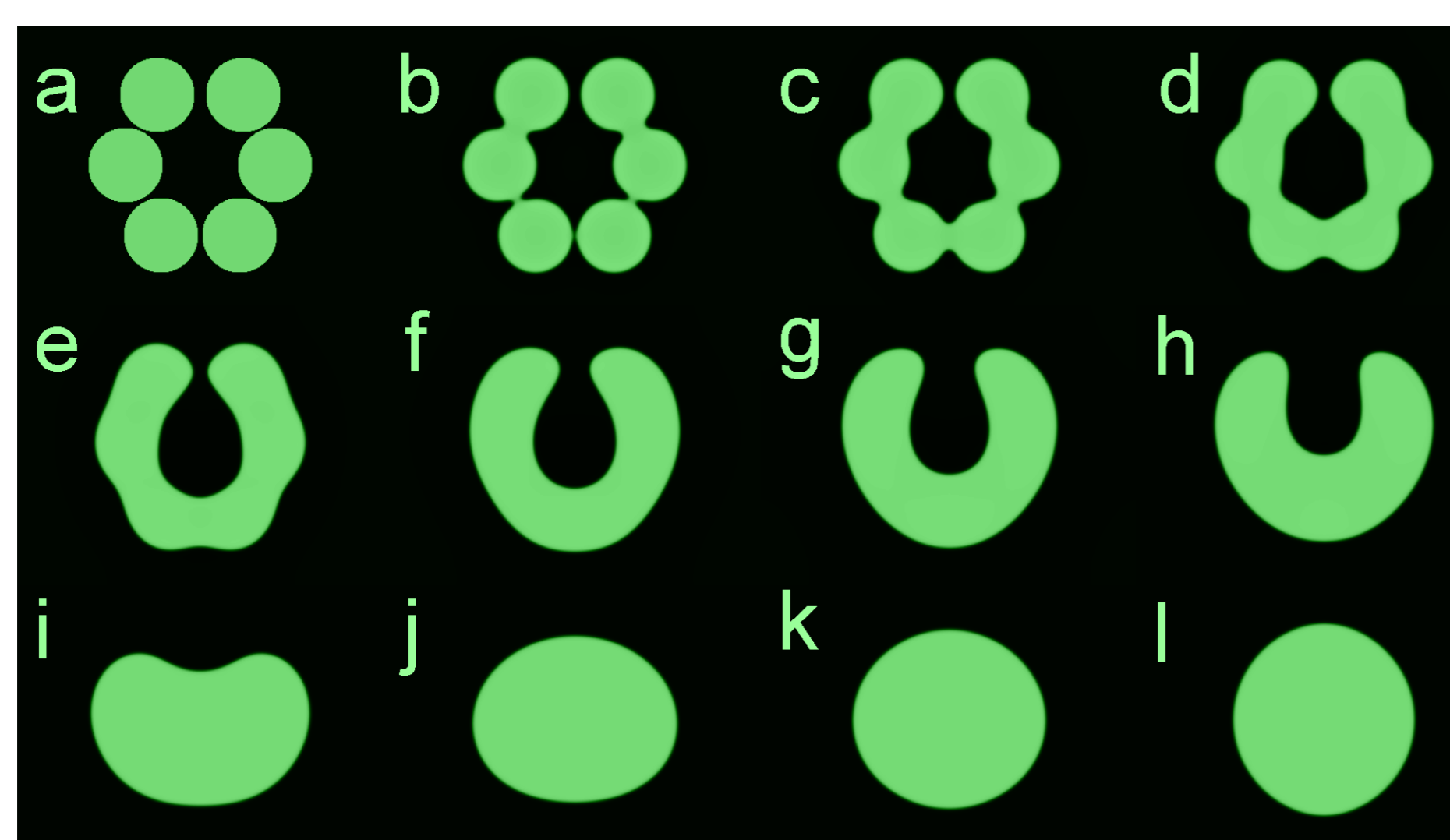
## Lattice Boltzmann (LB) simulations of droplet fusion<sup>4</sup>: the contact area describes the rate of fusion



## Cell cylinder printing<sup>5</sup> vs. LB simulations<sup>6</sup>



## How does a printing defect evolve?<sup>6</sup>



## Lattice Boltzmann model with flux limiters for two species<sup>3</sup>

$$f_{i,j}^{\sigma,n+1} = f_{i,j}^{\sigma,n} - CFL^\sigma \left[ F_{i,j+1/2}^{\sigma,n} - F_{i,j-1/2}^{\sigma,n} \right] - \frac{1}{\tau^\sigma} [f_i^\sigma - f_i^{\sigma,eq}] + \frac{\mathbf{F}^\sigma(\mathbf{r}, t)}{m^\sigma \chi(c^\sigma)^2} \cdot [\mathbf{e}_i^\sigma - \mathbf{u}(\mathbf{r}, t)] f_i^{\sigma,eq}$$

**BGK collision term**      **Force term**

$$\mathbf{F}^\sigma = - \sum_\lambda \omega^{\sigma\lambda} \nabla X^\lambda + \text{surfacetension terms} \quad X^\sigma(\mathbf{r}, t) = \frac{n^\sigma}{n^0 + n^1}$$

$$F_{i,j+1/2}^{\sigma,n} = f_{i,j}^{\sigma,n} + \frac{1}{2} (1 - CFL^\sigma) [f_{i,j+1}^{\sigma,n} - f_{i,j}^{\sigma,n}] \psi(\theta_{i,j}^{\sigma,n})$$

**Flux limiters terms**

$$F_{i,j-1/2}^{\sigma,n} = F_{i,(j-1)+1/2}^{\sigma,n} = f_{i,j-1}^{\sigma,n} + \frac{1}{2} (1 - CFL^\sigma) [f_{i,j}^{\sigma,n} - f_{i,j-1}^{\sigma,n}] \psi(\theta_{i,j-1}^{\sigma,n})$$

**MCD flux limiter scheme**

$$\psi(\theta_{i,j}^{\sigma,n}) = \begin{cases} 0 & , \theta_{i,j}^{\sigma,n} \leq 0 \\ \frac{2\theta_{i,j}^{\sigma,n}}{1 + \theta_{i,j}^{\sigma,n}} & , 0 \leq \theta_{i,j}^{\sigma,n} \leq \frac{1}{3} \\ \frac{1}{2} & , \frac{1}{3} \leq \theta_{i,j}^{\sigma,n} \leq 3 \\ 2 & , 3 \leq \theta_{i,j}^{\sigma,n} \end{cases}$$

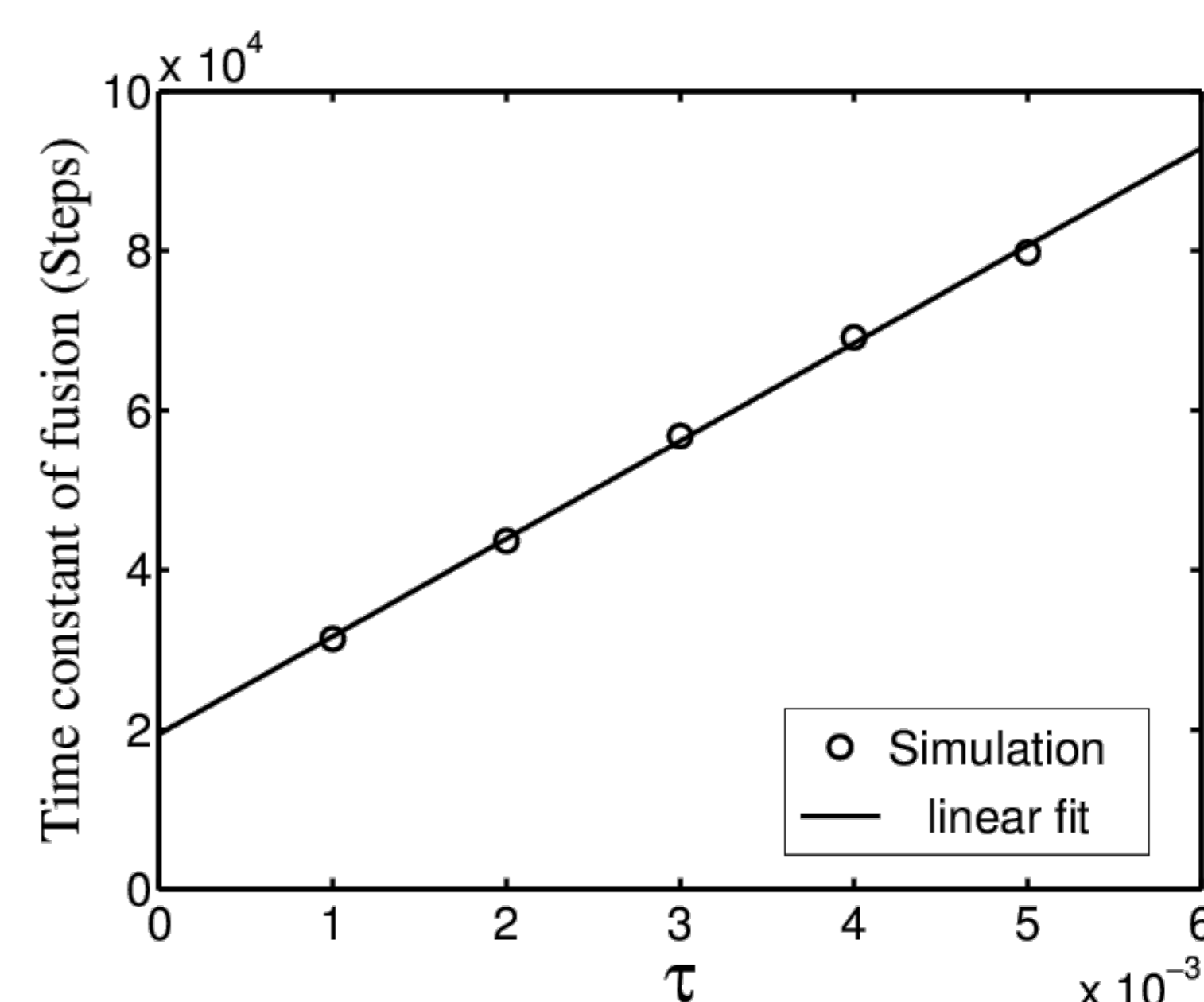
$$\theta_{i,j}^{\sigma,n} = \frac{f_{i,j}^{\sigma,n} - f_{i,j-1}^{\sigma,n}}{f_{i,j+1}^{\sigma,n} - f_{i,j}^{\sigma,n}}$$

The time constant of fusion is proportional to the relaxation time and should be set in relation with the known values of viscosity and surface tension<sup>4</sup>

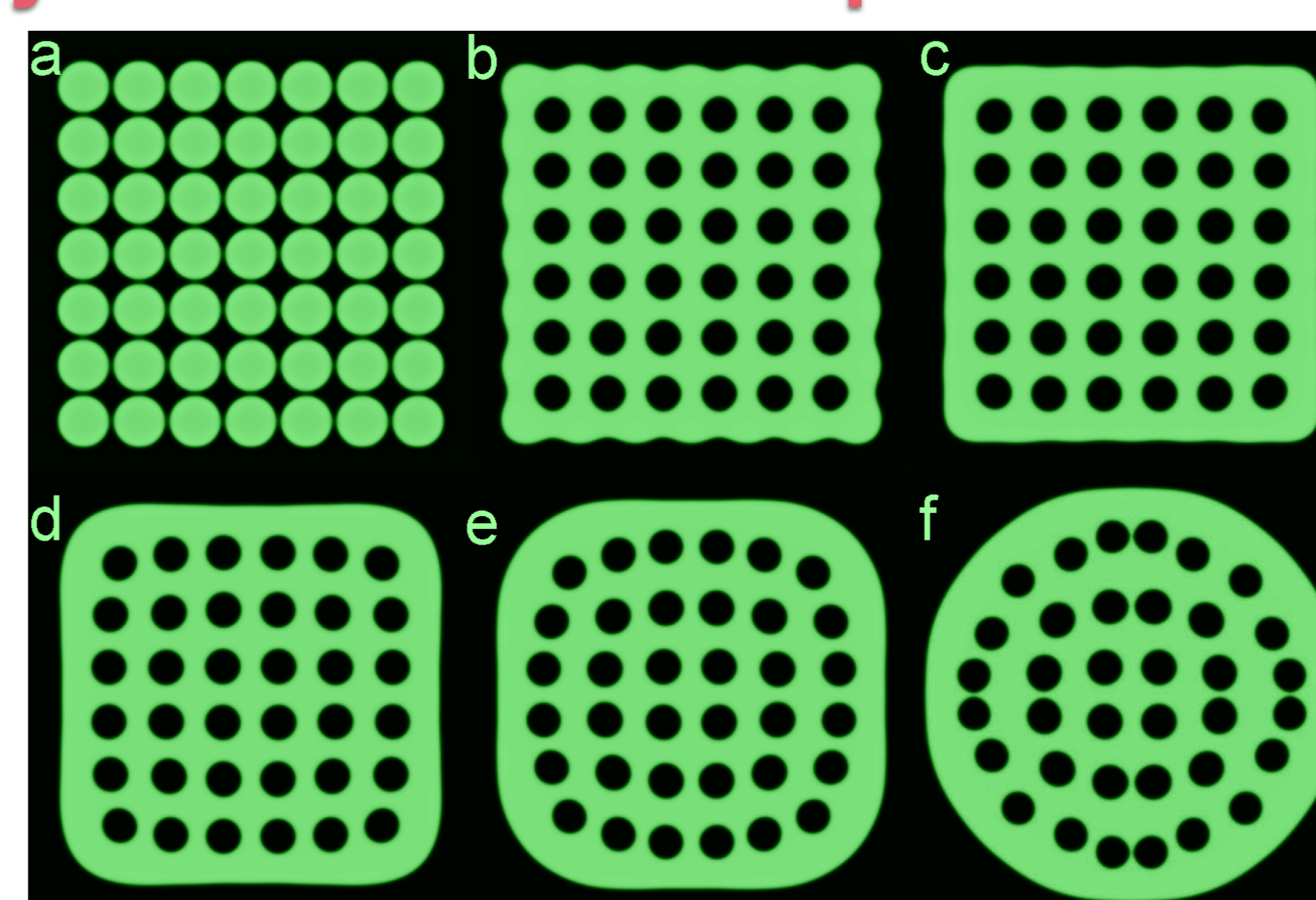
$$t_f \propto \frac{\eta}{\gamma} R_0$$

$$\frac{\eta}{\gamma} = \frac{\eta_0}{\gamma_0} (1 + b\tau)$$

$$\tau' = \frac{\eta'}{\gamma'} \tau + \frac{1}{b} \left( \frac{\eta'}{\gamma'} - 1 \right)$$



## Post-printing evolution of a rectangular stack of cell cylinders leads to a perfusable tissue<sup>6</sup>



## Perspectives

- Build simulation programs for predicting the shape evolution of heterotypic bioprinted tissue constructs in 3D.
- Account for viscoelastic behavior.
- Take into account cell division and cell death.

## References

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