Quadrature methods in lattice Boltzmann modelling

#### Victor E. Ambruș

Centre for Fundamental and Advanced Technical Research, Romanian Academy Bd. Mihai Viteazul 24, RO 300223 Timișoara, Romania

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# **Applications of lattice Boltzmann**

- Lattice Boltzmann is a method for solving the Boltzmann equation numerically.
- The Boltzmann equation is mesoscopic, i.e. the Knudsen number  $Kn = \frac{\lambda}{L}$  is non-negligible.
- At small Kn: multi-phase / multicomponent flows, where interface tracking is difficult macroscopically.
- At large Kn (beyond Navier-Stokes regime): microfluidics (microchannels, rarefied flows, flows in the ballistic regime).

H-theorem Maxwell-Boltzmann statistics Macroscopic equations Boundary conditions

# Boltzmann Equation

• Evolution equation of the one-particle distribution function  $f \equiv f(\mathbf{x}, \mathbf{p}, t)$ :

$$\partial_t f + \frac{1}{m} \mathbf{p} \cdot \nabla f + \mathbf{F} \cdot \nabla_{\mathbf{p}} f = J[f].$$

• The collision operator *J*[*f*] accounts for changes to *f* due to collisions:

$$J[f] = \int d^3p_* \, d^3p' \, d^3p'_* \, \delta^3(\mathbf{p} + \mathbf{p}_* - \mathbf{p}' - \mathbf{p}'_*) \, \delta(E + E_* - E' - E'_*)$$

$$\times \frac{d\sigma}{d\Omega} \frac{|\mathbf{p}' - \mathbf{p}'_*|}{m} (f'f'_* - ff_*).$$

• Assumptions:

- Only binary collisions need to be considered;
- Particle interactions are short ranged;
- Particle interaction durations are small;
- Interacting particles are completely uncorrelated (stosszahlansatz), i.e. f<sub>2</sub>(**p**<sub>1</sub>, **p**<sub>2</sub>, **x**<sub>1</sub>, **x**<sub>2</sub>, t) = f(**p**<sub>1</sub>, **x**<sub>1</sub>, t)f(**p**<sub>2</sub>, **x**<sub>2</sub>, t).

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#### H-theorem

- Under Boltzmann's assumptions, the second law of thermodynamics (of increasing entropy) is guaranteed.
- Consider the H-function:

$$H(t) = \int d^3x \int d^3p f \ln f.$$

• Its time derivative is:

$$\begin{aligned} \frac{dH}{dt} &= \int d^3x \int d^3p J[f](1+\ln f) \\ &= \frac{1}{4} \int d^3x \int d^3p \, d^3p_* \, d^3p' \, d^3p'_* \, \delta^3(\mathbf{p}+\mathbf{p}_*-\mathbf{p}'-\mathbf{p}'_*) \, \delta(E+E_*-E'-E'_*) \\ &\times \frac{d\sigma}{d\Omega} \frac{|\mathbf{p}'-\mathbf{p}'_*|}{m} (f'f'_*-ff_*)(\ln f+\ln f_*-\ln f'-\ln f'_*) \leq 0, \\ &\text{ since } (1-x) \ln x \leq 0. \end{aligned}$$
  
• Equality holds in (local) thermal equilibrium.

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#### Collision invariants

• Consider the following integrals:

$$\begin{split} J[f,\psi] &= \int d^3 p J[f] \,\psi \\ &= \frac{1}{4} \int d^3 p \, d^3 p_* \, d^3 p' \, d^3 p'_* \, \delta^3 (\mathbf{p} + \mathbf{p}_* - \mathbf{p}' - \mathbf{p}'_*) \,\delta(E + E_* - E' - E'_*) \\ &\times \frac{d\sigma}{d\Omega} \frac{\left| \mathbf{p}' - \mathbf{p}'_* \right|}{m} (f' f'_* - f f_*) (\psi + \psi_* - \psi' - \psi'_*). \end{split}$$

•  $\psi$  is a collision invariant if  $J[f, \psi] = 0$ .

• In the collisions considered here, the invariants are:

$$\psi \in \{1, \mathbf{p}, E\}.$$

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#### Maxwell-Boltzmann equilibrium

• The H-theorem can be written as:

$$\frac{dH}{dt} = \int d^3x J[f, \ln f + 1] \le 0.$$

• Equilibrium is attained when  $f(\mathbf{x}, \mathbf{p}, t) = f^{(eq)}(\mathbf{x}, \mathbf{p}, t)$ , such that:

$$\ln f^{(\text{eq})}(\mathbf{x}, \mathbf{p}, t) = A + \mathbf{B} \cdot \mathbf{p} + C E.$$

• Rearranging gives the Maxwell-Boltzmann equilibrium distribution:

$$f^{(\text{eq})}(\mathbf{x},\mathbf{p},t) = \frac{n}{(2\pi m K_B T)^{\frac{3}{2}}} \exp\left[-\frac{(\mathbf{p}-m\mathbf{u})^2}{2m K_B T}\right].$$

(from now on,  $K_B \equiv 1$ ).

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Moments of f

• The macroscopic properties of the fluid can be written in terms of moments of order *N* of *f*:

$$N = 0: \text{ number density:} \quad n = \int d^3 p f,$$

$$N = 1: \text{ velocity:} \quad \mathbf{u} = \frac{1}{nm} \int d^3 p f \mathbf{p},$$

$$N = 2: \text{ temperature:} \quad T = \frac{2}{3n} \int d^3 p f \frac{\boldsymbol{\xi}^2}{2m}, \quad (\boldsymbol{\xi} = \mathbf{p} - m\mathbf{u}),$$

$$\text{viscous tensor:} \quad \sigma_{\alpha\beta} = \int d^3 p \frac{\boldsymbol{\xi}_{\alpha} \boldsymbol{\xi}_{\beta}}{m} f - nT \delta_{\alpha\beta},$$

$$N = 3: \text{ heat flux:} \quad \mathbf{q} = \int d^3 p f \frac{\boldsymbol{\xi}^2}{2m} \frac{\boldsymbol{\xi}}{m}.$$

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# Transport equations

• Multiplying the Boltzmann equation:

$$\partial_t f + \frac{1}{m} \mathbf{p} \cdot \nabla f + \mathbf{F} \cdot \nabla_{\mathbf{p}} f = J[f],$$

by the collision invariants  $\psi \in \{1, \mathbf{p}, E\}$  and integrating over  $\mathbf{p}$  gives:

$$\partial_t n + \partial_\alpha (\rho u_\alpha) = 0,$$
  
$$\partial_t (\rho u_\alpha) + \partial_\beta (\rho u_\alpha u_\beta + nT \delta_{\alpha\beta} + \sigma_{\alpha\beta}) = nF_\alpha,$$
  
$$(\partial_t + \partial_\alpha u_\alpha) \left(\frac{3}{2}nT + \frac{\rho \mathbf{u}^2}{2}\right) + \partial_\alpha q_\alpha + \partial_\alpha \left[u_\beta \left(nT \delta_{\alpha\beta} + \sigma_{\alpha\beta}\right)\right] = nu_\alpha F_\alpha.$$

• The evolution of the moment of order *N* depends on the moment of order *N* + 1.

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#### BGK collision term

• In solving the Boltzmann equation (analytically or numerically), the collision term poses a challenge:

$$J[f] = \int d^{3}p_{*} d^{3}p' d^{3}p'_{*} \delta^{3}(\mathbf{p} + \mathbf{p}_{*} - \mathbf{p}' - \mathbf{p}'_{*}) \,\delta(E + E_{*} - E' - E'_{*})$$
$$\times \frac{d\sigma}{d\Omega} \frac{|\mathbf{p}' - \mathbf{p}'_{*}|}{m} (f'f'_{*} - ff_{*}).$$

• BGK approximation: the incoming particles are assumed to be distributed thermally:

$$f'f'_* = f^{(eq)}f^{(eq)}_* = f^{(eq)}f^{(eq)}_*.$$

• The integrals can now be performed to yield:

$$J_{\text{BGK}}[f] = -\frac{1}{\tau}[f - f^{(\text{eq})}],$$

where  $\tau$  is the relaxation time.

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# Chapman-Enskog expansion

• Typically, the relaxation time is chosen as  $(Kn = \lambda/L)$ :

$$\tau \sim \frac{n}{\mathrm{Kn}}.$$

• Chapman-Enskog assumptions:

$$f = f^{(0)} + f^{(1)} \operatorname{Kn} + f^{(2)} \operatorname{Kn}^2 + \dots,$$
  
$$f(\mathbf{x}, \mathbf{p}, t) \rightarrow f(\mathbf{x}, \mathbf{p}; n, \mathbf{u}, T).$$

• Since *f* now depends implicitly on *t*, the time derivative in the Boltzmann equation can be written using the chain rule:

$$\partial_t = \partial_t \rho \,\partial_\rho + \partial_t u_\alpha \,\partial_{u_\alpha} + \partial_t T \,\partial_T$$
$$= \partial_{t_0} + \operatorname{Kn} \partial_{t_1} + \operatorname{Kn}^2 \partial_{t_2} + \dots$$

• The time derivatives of *n*, **u** and *T* can be eliminated using the macroscopic equations.

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# Navier-Stokes equations

• Boltzmann equation at order *n* in Kn:

$$\sum_{j=0}^{n} \partial_{t_j} f^{(n-j)} + \frac{1}{m} \mathbf{p} \nabla f^{(n)} + \mathbf{F} \cdot \nabla_{\mathbf{p}} f^{(n)} = -\frac{1}{\tau'} \left[ f^{(n+1)} - f^{(eq)} \delta_{n,-1} \right],$$

where  $\tau' = \tau/Kn$ .

At order Kn<sup>-1</sup>: *f*<sup>(0)</sup> = *f*<sup>(eq)</sup>.
 At order Kn<sup>0</sup>:

$$f^{(1)} = -\tau' \left[ \partial_{t_0} f^{(0)} + \frac{1}{m} \mathbf{p} \nabla f^{(0)} + \mathbf{F} \nabla_{\mathbf{p}} f^{(0)} \right].$$

• Truncating at *O*(Kn) gives:

$$\begin{split} \sigma_{\alpha\beta} &= -\tau nT \left[ \partial_{\alpha} u_{\beta} + \partial_{\beta} u_{\alpha} - \frac{2}{D} \partial_{\gamma} u_{\gamma} \right], \\ q_{\alpha} &= -\frac{1}{\Pr} \frac{D+2}{2m} \tau nT \partial_{\alpha} T, \end{split}$$

where the Prandtl number Pr = 1 in the BGK model.

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## Shakhov collision term

• To recover the Prandtl number Pr = 2/3 for ideal monatomic gases, the Shakhov collision term must be used:

$$J[f] = -\frac{1}{\tau} \left[ f - f^{(\text{eq})}(1+\$) \right],$$
$$\$ = \frac{1 - \Pr}{nT^2} \left[ \frac{\xi^2}{(D+2)mT} - 1 \right] \xi \cdot \mathbf{q}$$

- Through the Chapman-Enskog expansion, the recovery of the Navier-Stokes-Fourier equations requires moments of up to order N = 6 of  $f^{(eq)}$ .
- Moments of  $f^{(eq)}$  of order up to N = 6 required to recover the Navier-Stokes equations in the Shakhov model.

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# Boundary conditions for the distribution function

Due to the particle – wall interaction, reflected particles carry some information that belongs to the wall.







bounce back

specular reflection

diffuse reflection

Diffuse reflection the distribution function of *reflected* particles is identical to the

Maxwellian distribution function  $f^{(eq)}(\mathbf{u}_{wall}, T_{wall})$ Microfluidics  $Kn = \lambda/L$  is non-negligible

- $\Rightarrow$  velocity slip  $u_{slip}$
- $\Rightarrow$  temperature jump  $T_{jump}$

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# Diffuse reflection boundary conditions

• The diffuse reflection boundary conditions require:

$$f(\mathbf{x}_{\mathrm{w}},\mathbf{p},t) = f^{(\mathrm{eq})}(n_{\mathrm{w}},\mathbf{u}_{\mathrm{w}},T_{\mathrm{w}}) \qquad (\mathbf{p}\cdot\chi<0),$$

where  $\chi$  is the outwards-directed normal to the boundary.

• The density *n*<sub>w</sub> is fixed by imposing zero flux through the boundary:

$$\int_{\mathbf{p}\cdot\chi>0} d^3p f\left(\mathbf{p}\cdot\chi\right) = -\int_{\mathbf{p}\cdot\chi<0} d^3p f^{(\text{eq})}\left(\mathbf{p}\cdot\chi\right)$$

• Diffuse reflection requires the computation of integrals of f and  $f^{(eq)}$  over half of the momentum space.

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# Example: ballistic regime of Couette flow

- Flow between parallel plates  $(x_t = -x_b = 0.5)$  moving along *y*.
- Diffuse reflection on the *x* axis.
- In the ballistic regime, the gas is effectively collisionless:

$$\partial_t f + \frac{\mathbf{p}}{m} \nabla f = 0.$$

• Ballistic regime (Kn  $\rightarrow \infty$ ) solution:



• Half-range models required to capture the discontinuous character of *f*.

Simulations performed using PETSc 3.1 on BlueGene cluster - collaboration with Prof. Dana Petcu, West University of Timișoara, Romania.





Orthogonal polynomials Quadrature methods

# Importance of moments of $f^{(eq)}$

• To construct numerically a solution of the Boltzmann equation:

$$\partial_t f + \frac{1}{m} \mathbf{p} \cdot \nabla f + \mathbf{F} \cdot \nabla_{\mathbf{p}} f = J[f],$$

time, space and the momentum must be discretised.

• The key is to preserve the moments of  $f^{(eq)}$ :

$$\int d^3p f^{(\text{eq})} P_n(\mathbf{p}) = \sum_k f_k^{(\text{eq})} P_n(\mathbf{p}_k),$$

where  $P_n(\mathbf{p})$  is a polynomial of order *n* in **p**.

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# Orthogonal expansion (1D)

• Consider the set of orthogonal polynomials  $\{\phi_{\ell}(x)\}$ :

$$\int dx \,\omega(x) \,\phi_{\ell}(x) \,\phi_{\ell'}(x) = \delta_{\ell\ell'}.$$

• The distribution function *f* can be written as:

$$f=\omega(\overline{p})\sum_{\ell=0}^{\infty}\mathcal{F}_{\ell}\,\phi_{\ell}(\overline{p})\qquad (\overline{p}=p/p_0),$$

where  $p_0$  is an arbitrary reference momentum.

• Since  $\phi_{N+1}$  is orthogonal to  $\phi_{\ell}$  for all  $\ell \leq N$ , the first *N* moments of *f* are fully contained in the coefficients  $\mathcal{F}_{\ell}$  ( $0 \leq \ell \leq N$ ).

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#### Orthogonal expansion (1D)

• In general,

$$\langle \phi_{\ell}, \phi_{\ell'} \rangle \equiv \int dx \, \omega(x) \, \phi_{\ell}(x) \, \phi_{\ell'}(x) = \delta_{\ell\ell'}.$$

• The distribution function *f* can be written as:

$$f = \omega(\overline{p}) \sum_{\ell=0}^{\infty} \mathcal{F}_{\ell} \phi_{\ell}(\overline{p}) \qquad (\overline{p} = p/p_0),$$

where  $p_0$  is an arbitrary reference momentum.

• Since  $\phi_{N+1}$  is orthogonal to  $\phi_{\ell}$  for all  $\ell \leq N$ , the first *N* moments of *f* are fully contained in the coefficients  $\mathcal{F}_{\ell}$  ( $0 \leq \ell \leq N$ ).

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# Orthogonal polynomials

• For any set of orthogonal polynomials  $\phi_{\ell}(x)$  satisfy the following recursion:

$$\phi_{\ell+1}(x) = (a_{\ell}x + b_{\ell})\phi_{\ell}(x) + c_{\ell}\phi_{\ell-1}(x),$$
$$a_{\ell} = A_{\ell+1}/A_{\ell}, \qquad b_{\ell} = -a_{\ell} \langle x\phi_{\ell}, \phi_{\ell} \rangle, \qquad c_{\ell} = -\frac{a_{\ell}}{a_{\ell-1}},$$

where  $A_{\ell}$  is the coefficient of the leading order term in  $\mathfrak{h}_{\ell}$ . • The unknown  $A_{\ell+1}$  (hence,  $a_{\ell}$ ) can be found using:

$$\frac{1}{a_{\ell}^2} = \langle x\phi_{\ell}, x\phi_{\ell} \rangle - \langle x\phi_{\ell}, \phi_{\ell} \rangle - \frac{1}{a_{\ell-1}^2}$$

Recursion method more accurate than Gram-Schmidt.

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## Projection of the Boltzmann equation (free, 1D)

• Consider the free one-dimentional Boltzmann equation with the BGK collision term:

$$\partial_t f + \frac{p}{m} \partial_x f = -\frac{1}{\tau} (f - f^{(\text{eq})}).$$

• Consider coefficient of  $\phi_{\ell}$ :

$$\partial_t \mathcal{F}_{\ell} + \frac{p_0}{m} \partial_x \left( \frac{\mathcal{F}_{\ell-1}}{a_{\ell-1}} - \frac{b_{\ell}}{a_{\ell}} \mathcal{F}_{\ell} - \frac{c_{\ell+1}}{a_{\ell+1}} \mathcal{F}_{\ell+1} \right) = -\frac{1}{\tau} \left( \mathcal{F}_{\ell} - \mathcal{F}_{\ell}^{\text{eq}} \right).$$

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# Truncation of the Boltzmann equation (free, 1D)

• Consider the truncated distribution function:

$$f^{(N)} = \omega(\overline{p}) \sum_{\ell=0}^{N} \mathcal{F}_{\ell} \phi_{\ell}(\overline{p}).$$

• Boltzmann equation for true *f* up to order *N*:

$$\sum_{\ell=0}^{N} \phi_{\ell}(\overline{p}) \left\{ \partial_{t} \mathcal{F}_{\ell} + \frac{p_{0}}{m} \partial_{x} \left( \frac{\mathcal{F}_{\ell-1}}{a_{\ell-1}} - \frac{b_{\ell}}{a_{\ell}} \mathcal{F}_{\ell} - \frac{c_{\ell+1}}{a_{\ell+1}} \mathcal{F}_{\ell+1} \right) + \frac{1}{\tau} \left( \mathcal{F}_{\ell} - \mathcal{F}_{\ell}^{eq} \right) \right\} = 0.$$

• Boltzmann equation for truncated  $f^{(N)}$ :

$$\partial_t f^{(N)} + \frac{p}{m} \partial_x f^{(N)} + \frac{1}{\tau} [f^{(N)} - f^{(\text{eq})}_{(N)}] = \epsilon_N,$$

where

$$\epsilon_N = \omega(\overline{p}) \frac{p_0}{m} \left[ \frac{c_{N+1}}{a_{N+1}} \phi_N(\overline{p}) \partial_x \mathcal{F}_{N+1} + \frac{1}{a_N} \phi_{N+1}(\overline{p}) \partial_x \mathcal{F}_N \right].$$

F. Pascal, S. Blanco, V. Sofonea, S. Olivier, R. Fournier, L. Guillaume, V. Ambruș, in preparation.

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### Quadrature methods

• According to the Gauss quadrature method,

$$\int dx \,\omega(x) \, P_n(x) = \sum_{k=1}^Q w_k \, P_(x_k)$$

is exact for Q > 2n.

- The quadrature points  $x_k$  are the Q roots  $\phi_Q(x)$ .
- The quadrature weights  $w_k$  are given by:

$$w_k = -\frac{A_{m+1}}{A_m \phi_{m+1}(x_k) \phi'_m(x_k)}.$$

• Choosing Q = N + 1 and initialising the distribution function only up to order N (i.e.  $\mathcal{F}_{N+1} = 0$ ) ensures that  $\epsilon_N = 0$ .

$$\epsilon_N = \omega(\overline{p}) \frac{p_0}{m} \left[ \frac{c_{N+1}}{a_{N+1}} \phi_N(\overline{p}) \partial_x \mathcal{F}_{N+1} + \frac{1}{a_N} \phi_{N+1}(\overline{p}) \partial_x \mathcal{F}_N \right] = 0.$$

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#### Formulation of half-space problem

• Rewrite integrals over the whole momentum space in terms of half-space integrals:

$$\int_{-\infty}^{\infty} dp f(p) P_n(p) = \int_0^{\infty} dp [f(p) P_n(p) + f(-p) P_n(-p)],$$

• The half-space integrals are replaced by quadrature sums:

$$\int_0^\infty dx\,\omega(x)P_n(x)=\sum_{k=1}^Q w_kP(x_k),$$

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#### Formulation of half-space problem

• The quadrature method can be implemented using Laguerre<sup>†</sup>:

$$\omega(x) = e^{-x}, \qquad w_k = \frac{x_k}{(Q+1)^2 [L_{Q+1}(x_k)]^2},$$

• ... or half-range Hermite polynomials\*

$$\omega(x) = \frac{1}{\sqrt{2\pi}} e^{-x^2/2}, \qquad w_k = \frac{A_{Q+1}}{A_Q \mathfrak{h}_{Q+1}(x_k) \mathfrak{h}'_Q(x_k)}$$

<sup>+</sup> V. E. Ambruş, V. Sofonea, Phys. Rev. E 89 (2014) 041301(R).
<sup>\*</sup> G.P. Ghiroldi, L. Gibelli, Journal of Computational Physics 258 (2014) 568.

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# Temperature profile for Couette flow at Kn=0.5

Comparison between full-space (HLB and SLB) and half-space (LLB and HHLB) models:

*T* across the channel

*T* at the centre of the channel



 $(u_{walls}=\pm 0.42$  ,  $T_{walls}=1.0$  ,  $\delta s=10^{-2}$  ,  $\delta t=10^{-4}$  , Kn=0.5 )

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#### Couette flow: comparison with DSMC



- DSMC (for Kn = 0.1 and 0.5) vs. LLB (lines) and HHLB (points) at Kn = 0.1, 0.5 and 1.0.
- Discrepancy in temperature profile due to incompatibility between the Shakhov model and the hard-sphere molecules used for DSMC.

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# Couette flow: ballistic regime (Kn $\rightarrow \infty$ )

• In the ballistic regime, all moments are constant.

LLB\*/HHLB results at  $T_b = 1.0$ ,  $T_t = 10.0$  and  $u_w = 0.42$ :

Model	Velocities	Т	u <sub>y</sub>	$q_x$	$q_y$
LLB(2, 2, 2)	64	2.910987	-0.218165	-6.305084	1.414574
HHLB(2, 2, 2)	64	1.943523	-0.216613	-2.807558	0.977046
LLB(3, 3, 3)	216	3.205209	-0.218187	-11.40061	3.700024
HHLB(3,3,3)	216	3.205236	-0.218184	-10.45152	2.787300
<b>LLB</b> (4, 4, 4)	512	3.205209	-0.218187	-11.02230	3.477877
<b>HHLB</b> (4, 4, 4)	512	3.205209	-0.218187	-11.02230	3.477871
Analytic		3.205209	-0.218187	-11.02227	3.477866

- Half-range models recover the ballistic regime with 512 velocities.
- Full-space models break down at large T differences as  $Kn \rightarrow \infty$ .

V. E. Ambruș, V. Sofonea, Phys. Rev. E 89, 041301(R) (2014)

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#### Force term in LLB

- In the Boltzmann equation, the force term involves  $\mathbf{F} \cdot \nabla_{\mathbf{p}} f$ .
- After discretisation,  $\nabla_{\mathbf{p}} f$  is replaced with a suitable expansion.
- The EQ (equilibrium) method:

$$\nabla_{\mathbf{p}} f \simeq \nabla_{\mathbf{p}} f^{(\mathrm{eq})} = \frac{\mathbf{p} - m\mathbf{u}}{mT} f^{(\mathrm{eq})},$$

which works if the fluid is not far from equilibrium (small Kn).
The SC (Shan-Chen) method<sup>+</sup>:

$$f = w(\overline{p}) \sum_{\ell} \mathcal{F}_{\ell} \phi_{\ell}(\overline{p}), \qquad \partial_{p} f = w(\overline{p}) \sum_{\ell} \mathcal{F}_{\ell}^{p} \phi_{\ell}(\overline{p}).$$

• The coefficients  $\mathcal{F}_{\ell}^{p}$  for  $\partial_{p}f$  can be calculated using  $\mathcal{F}_{\ell}$ .

<sup>+</sup> N. S. Martys, X. Shan, H. Chen, Phys. Rev. E 58, 6855 (1998).X. W. Shan, X. F. Yuan, H. D. Chen, J. Fluid. Mech. 550, 413 (2006).

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# Application: Poiseuille flow

- Flow between parallel stationary plates driven by  $\mathbf{a} = (0, a_y, 0)$ , with  $a_y = 0.1$ .
- $x_t = -x_b = 0.5$
- Temperature of plates:  $T_b = T_t = 1.0$
- Diffuse reflection on the *x* axis
- Micro-fluidics effects: temperature jump, velocity slip, temperature dip.
- SC required for the temperature dip.
- Analytical results\* in the ballistic regime show that
  - *T* is parabolic using SC:
    - $T = T_0 + x^2 \delta T$
  - *T* is flat using EQ.



Simulations done using PETSc 3.4 at BlueGene cluster - collaboration with Prof. Daniela Petcu, West University of Timișoara, Romania.

\* V. E. Ambruș, V. Sofonea, Interfacial Phenomena and heat transfer, with editors.

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#### EQ vs SC: Poiseuille flow



Good agreement between EQ and SC at small Kn for *T* and  $q_y$  and throughout the Kn range for  $u_y$  and  $q_x$ . EQ does not recover the temperature dip.

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# EQ vs SC: dip in Poiseuille flow temperature profile

Temperature dip at Kn > 0.1 requires SC.

1% accuracy achieved by:



Kn	Vel (LLB)	Vel (HHLB)
≤ 0.1	2744	512
0.25	2744	2744
0.5	2744	4096
1.0	4096	4096
$\infty$	2744	2744

Temperature profile across the channel in Poiseuille flow: comparison between EQ (points) and SC (lines) models.

$$(a_y=0.1$$
 ,  $T_{walls}=1.0$  ,  $\delta s=10^{-2}$  ,  $\delta t=10^{-5})$ 

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# EQ vs SC: Ballistic regime

Temperature in the ballistic regime.

#### EQ method:

#### SC method:



The SC profile is parabolic, in agreement with \* and with analytic results<sup>+</sup>. The EQ profile is constant<sup>+</sup>.

\* J. Meng, L. Wu, J. M. Reese, Y. Zhang, J. Comp. Phys. **251** (2013) 383.

<sup>+</sup> V. E. Ambruș, V. Sofonea, Interfacial Phenomena and heat transfer, with editors.

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# Tissue growth - motivation

- Tissue engineering aim to replace or repair damaged tissues, even organs.
- Computational methods are extremely valuable for understanding morphogenesis.
- In mesoscale (LB), the system is simulated using two isothermal and incompressible components.
- Simulation results are validated by comparison to experimental data<sup>†</sup>.

<sup>+</sup> C. Norotte, F. Marga, L. E. Niklason, G. Forgacs, Biomaterials 30 (2009) 5910.

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# Simulation of tissue growth using a two-component flow

• Consider a 2D two-component flow ( $\sigma = 0, 1$ ):

$$\partial_t f^{\sigma} + \frac{\mathbf{p}}{m} \nabla f^{\sigma} - \mathbf{F}^{\sigma} \nabla_{\mathbf{p}} f = -\frac{1}{\tau^{\sigma}} \left[ f^{\sigma} - f^{\sigma, \text{eq}} \right].$$

- D2Q9 model used.
- EQ method used for the momentum gradient:

$$\mathbf{F}^{\sigma} \nabla_{\mathbf{p}} f \to \mathbf{F} \cdot \frac{\mathbf{p} - m\mathbf{u}}{mT} f^{\sigma, \mathrm{eq}}.$$

• The inter-particle interaction of strength  $\omega$  and the surface tension described by  $\kappa$  is modelled as:

$$\mathbf{F}^{\sigma} = -\omega \nabla X^{1-\sigma} + \kappa \nabla (\nabla^2 X^{\sigma}),$$

where  $X^{\sigma} = n^{\sigma}/(n^0 + n^1)$  is the mole fraction of species  $\sigma$ .

A. Cristea, A. Neagu, Biofabrication, under revision.

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# Fusion of multicellular cylinders in a hexagonal arrangement



Snapshots of (2D) evolution of cross-section of a 3D tubular structure: initial configuration (a) and after  $5 \times 10^3$  (b),  $1 \times 10^4$  (c),  $1.5 \times 10^4$  (d),  $2.5 \times 10^4$  (e),  $5 \times 10^4$  (f),  $7.5 \times 10^4$  (g) and  $1 \times 10^5$  (h) time steps.

A. Cristea, A. Neagu, Biofabrication, under revision.

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#### Evolution of printing defect



Snapshots of (2D) evolution of printing defect: initial configuration (a) and after  $5 \times 10^3$  (b),  $1 \times 10^4$  (c),  $1.5 \times 10^4$  (d),  $2.5 \times 10^4$  (e),  $5 \times 10^4$  (f),  $7.5 \times 10^4$  (g),  $1 \times 10^5$  (h),  $1.5 \times 10^5$  (i),  $2 \times 10^5$  (j),  $2.5 \times 10^5$  (k) and  $5 \times 10^5$  (l) time steps. [A. Cristea, A. Neagu, Biofabrication, under revision.]

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#### Phase separation using lattice Bolzmann

• Phase separation achieved by changing the ideal gas equation of state to that of van der Waals gases, by adding a force term:

$$\mathbf{F} = \frac{1}{n} \nabla (p_i - p_w) + \kappa \nabla (\nabla^2 n).$$

• The ideal pressure  $p_i = nT$  is changed to the van der Waals pressure:

$$p_w = \frac{3nT}{3-n} - \frac{9}{8}n^2.$$

• No interface tracking required.

T. Biciușcă, V. Sofonea, Proceedings of DSFD-2014 (under revision).

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#### Liquid-vapour phase diagram



V. E. Ambruş Half-range LB models

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Phase separation





iter = 500000

iter = 1000000

Half-range LB models

V. E. Ambruș

iter = 2000000

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Phase separation





iter = 200000

iter = 500000

iter = 600000

V. E. Ambruș

Half-range LB models

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#### $\rho_{mean} = 0.90$ : Evolution of the mean drop size $1/\mathcal{P}$



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T = 0.85: Liquid drops separation on a 3D lattice with 128 x 128 x 128 nodes







iter = 10000



iter = 160000



- Quadrature methods provide a systematic way of increasing the accuracy of lattice Boltzmann simulations.
- Half-space quadratures essential for the implementation of diffuse-reflection boundary conditions.
- EQ implementation of force term ( $\nabla_{\mathbf{p}} f \sim \nabla_{p} f^{(\mathrm{eq})}$ ) inaccurate (no temperature dip in Poiseuille flow; less accurate van der Waals phase diagram), compared to NS implementation.
- Multiphase and multicomponent flows can be simulated by modelling inter-particle forces.